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Dipartimento di Ingegneria Chimica,
Gestionale, Informatica, Meccanica (DICGIM)

Reverse Electrodialysis Process: Analysis of Optimal Conditions for Process Scale-up

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Desalination for the Environment, Clean Water and Energy
Cyprus, 11 -15 May 2014



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Outline

- **Introduction**

- Principle of Reverse Eletrodialysis
- Non-ideal phenomena
- Focus of the work

- **Modelling**

- Model assumptions
- Governing equations
- Process simulator
- Validation

- **Results**

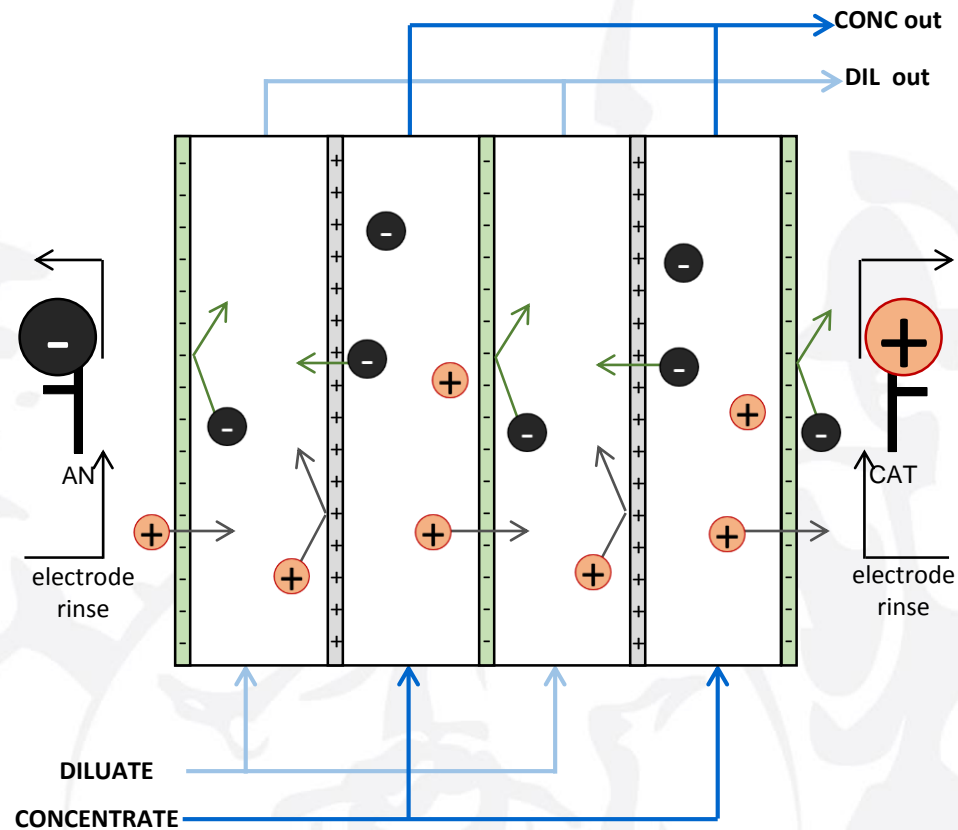
- Different path length for diluate/concentrate
- Exploring the optimal operating conditions
- Simulation of large-scale pilot
- Process simulation for a 3 RED units plant

- **Conclusions**



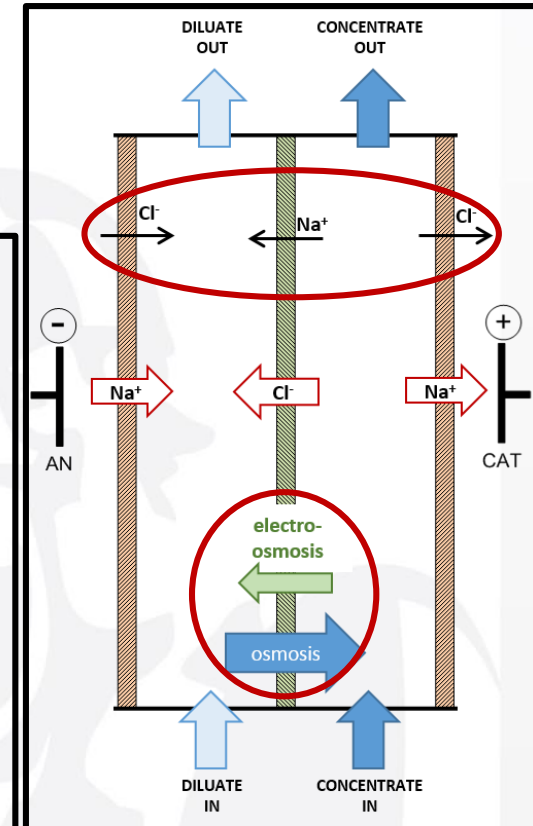
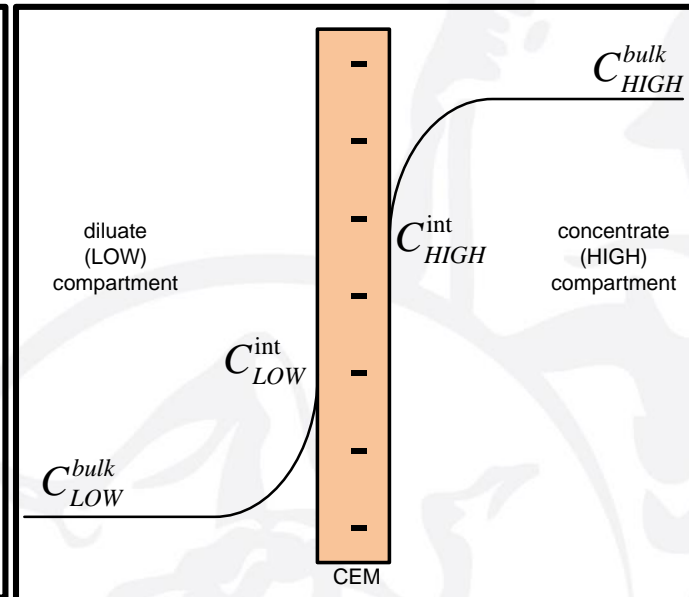
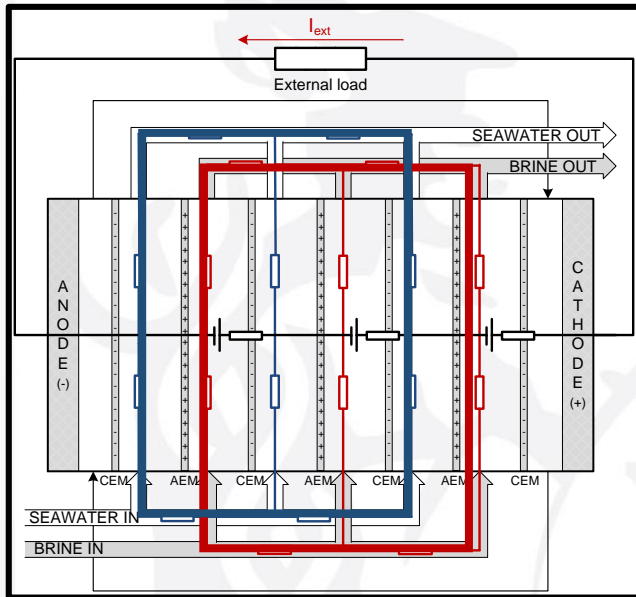
Principle of Reverse Electrodialysis

direct conversion of
SALINITY GRADIENT ENERGY → **ELECTRICITY**



Non-ideal phenomena

- *non-ideal IEMs permselectivity*
- *Solvent transport through IEMs*
- *Concentration polarisation phenomena*
- *Parasitic currents*

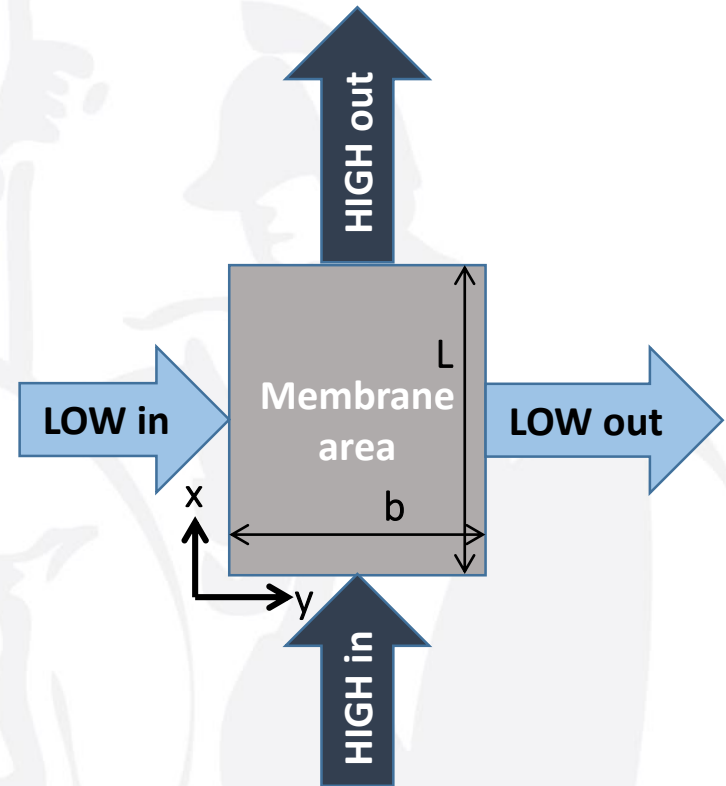
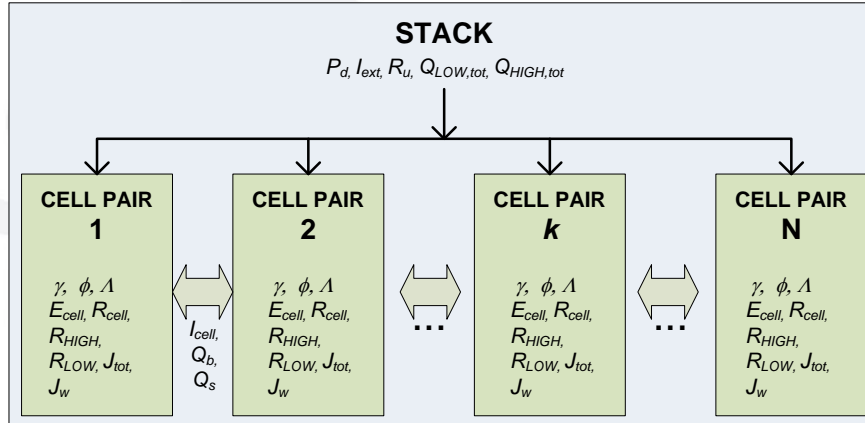


Focus of the work

GOAL:

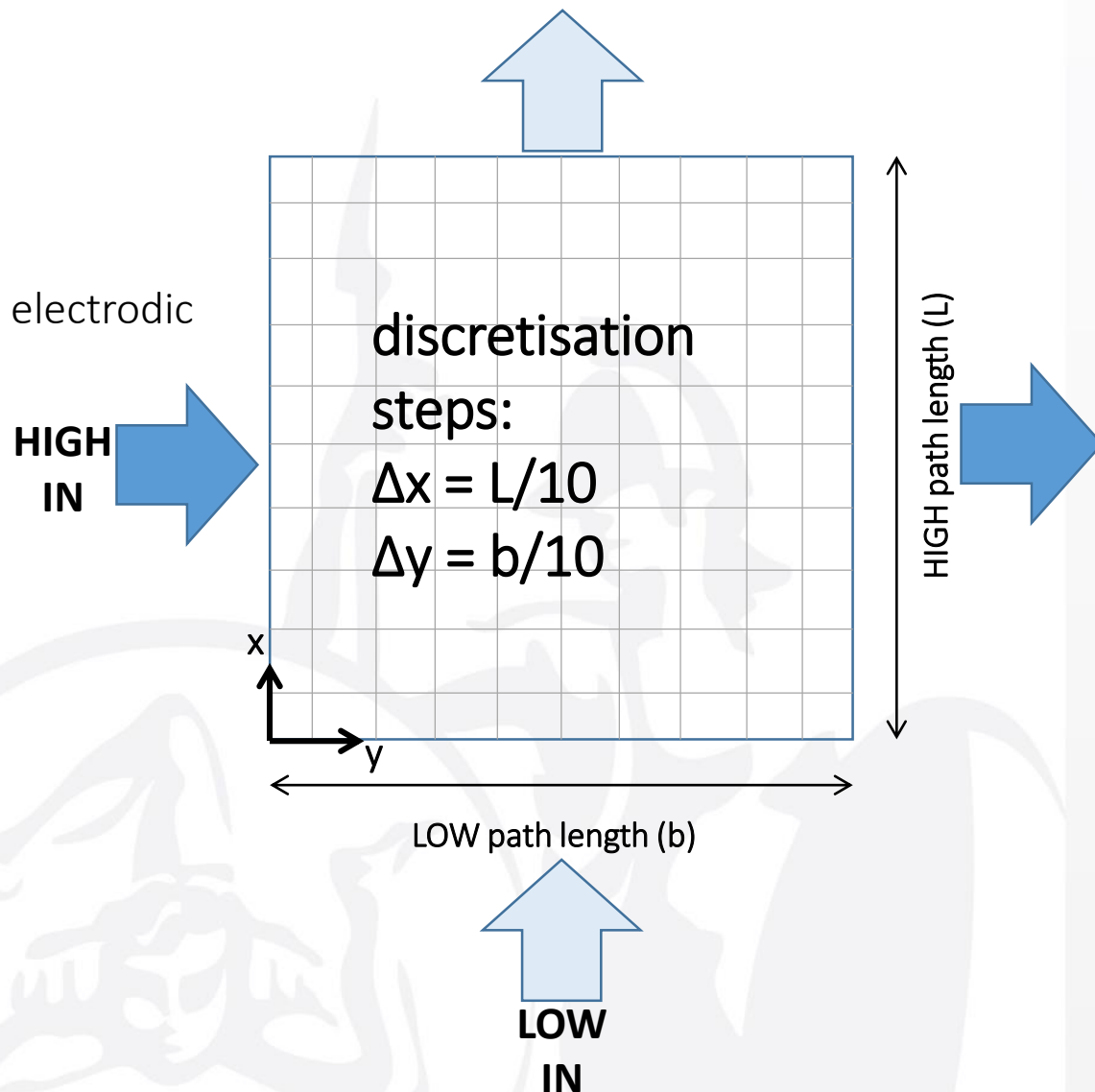
Development of a **simulator for RED Process** using **sea/brackish water** and **brine** as feed solutions

Multi-Scale Modelling Approach:



Model assumptions

- ✓ 2D model
- ✓ pure NaCl aqueous solutions
- ✓ negligible parasitic currents for electrodic solution



Governing equations

- solutions properties

- Activity and osmotic coefficients
- Equivalent conductivity
- Density
- Viscosity

- Electric variables

- Cell pair voltage
- Solutions and membranes resistance
- Parasitic currents in manifolds

- Transport eq. through membranes

- Salt transport
- Solvent transport

- Mass balance and polarisation phenomena

- Response variables

- Gross power

$$P = I_{ext}^2 R_u$$

- Pumping power

$$P_{pump} = \frac{\Delta P_{HIGH} Q_{HIGH}^{tot} + \Delta P_{LOW} Q_{LOW}^{tot}}{\eta_p}$$

- Gross Power density

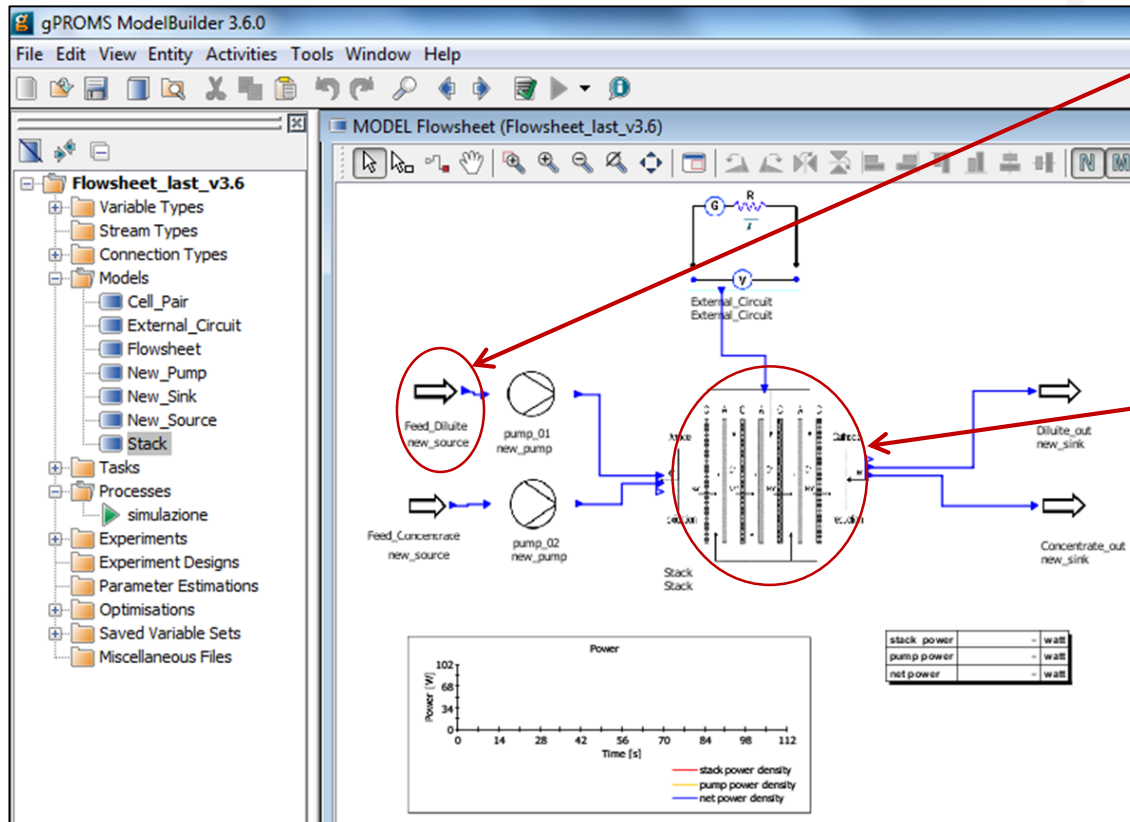
$$P_d = \frac{1}{N} \left(\frac{I_{ext}}{A} \right)^2 R_u$$

- Net Power density

$$P_{d.net} = P_d - \frac{P_{pump}}{N A}$$

Process simulator

- Process simulator GUI in gPROMS



Feed_Diluite (New_Source)

Specify

- pressure: 1.01325E5 Pa
- temperature: 313 K
- solution: other (concentration must be specified)

Physical conditions and type of solution: _____ Flowrate: _____
Concentration (for 'other' solution): _____

OK Cancel Reset All

Stack (Stack)

Specify

- cell width: 0.1 m
- flow path length: 0.1 m
- spacer in dilute compartments: Deukum 270 micron, parallel type
- spacer in concentrate compartments: Same of dilute compartments

Cell Geometry Membrane Properties Other

OK Cancel Reset All

Stack (Stack)

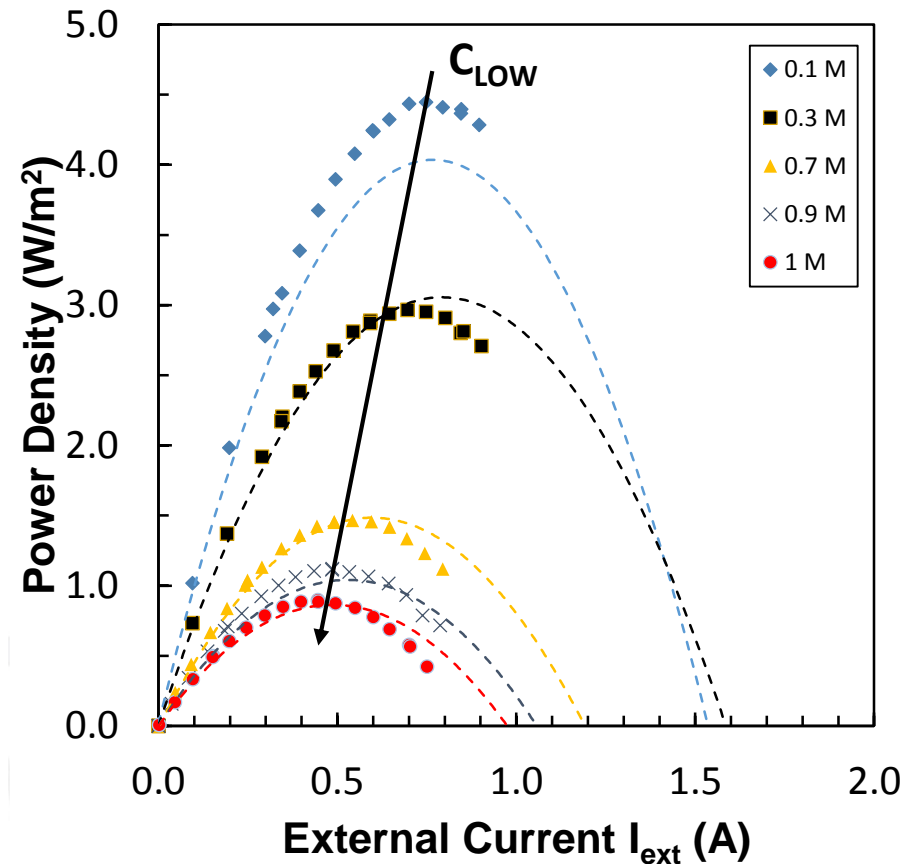
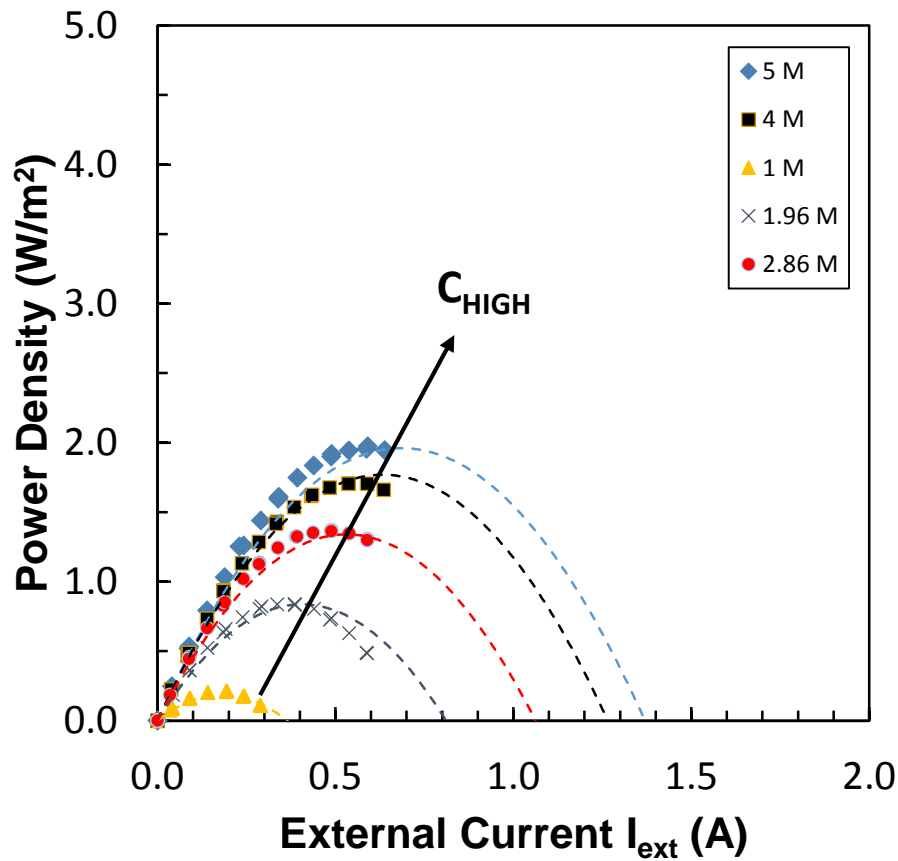
Specify

- anionic membrane permselectivity: 0.65
- cationic membrane permselectivity: 0.9
- membrane thickness: 1.25E-6 m
- areal resistance of anionic membrane: 1.83E-4 ohm*m^2
- areal resistance of cationic membrane: 2.55E-4 ohm*m^2
- IEM water permeability: 1.34E-14 m^3/m^2*s*Pa

Cell Geometry Membrane Properties Other Stack Specifications

OK Cancel Reset All

Validation on a lab-scale unit








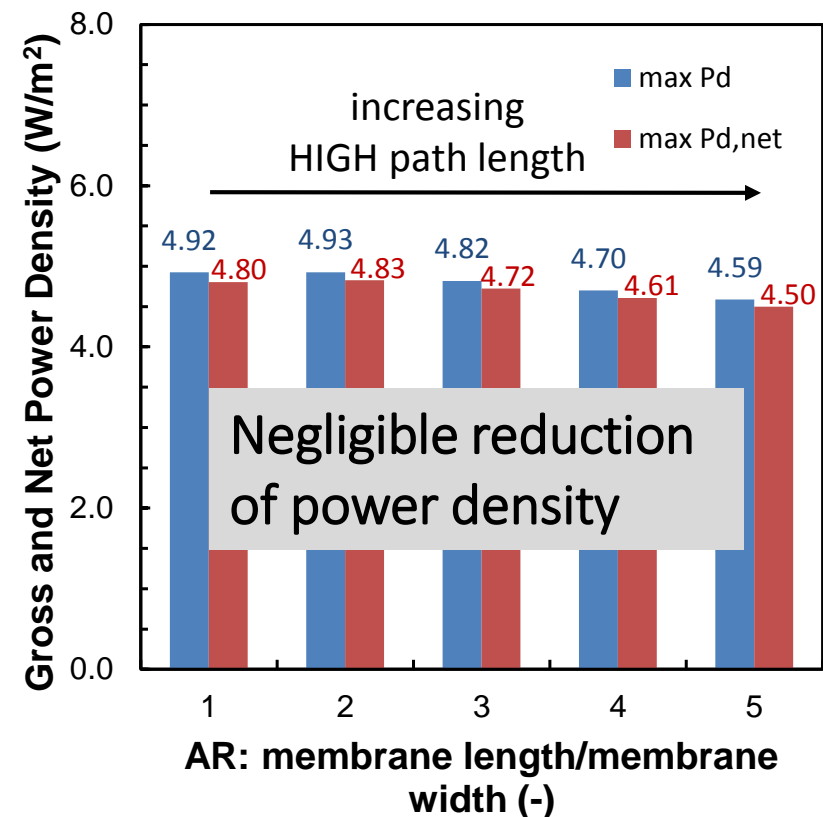
Experimental (points) and simulated (lines) data for a 50-cells stack equipped with Fujifilm membranes, Deukum 270 μm spacers; feed flow velocity: 1 cm/s; $T=20^\circ\text{C}$. Experimental data collected at VITO (Belgium).

Different path length for diluate/concentrate (1/2)

- Effect of Aspect Ratio on Power Density

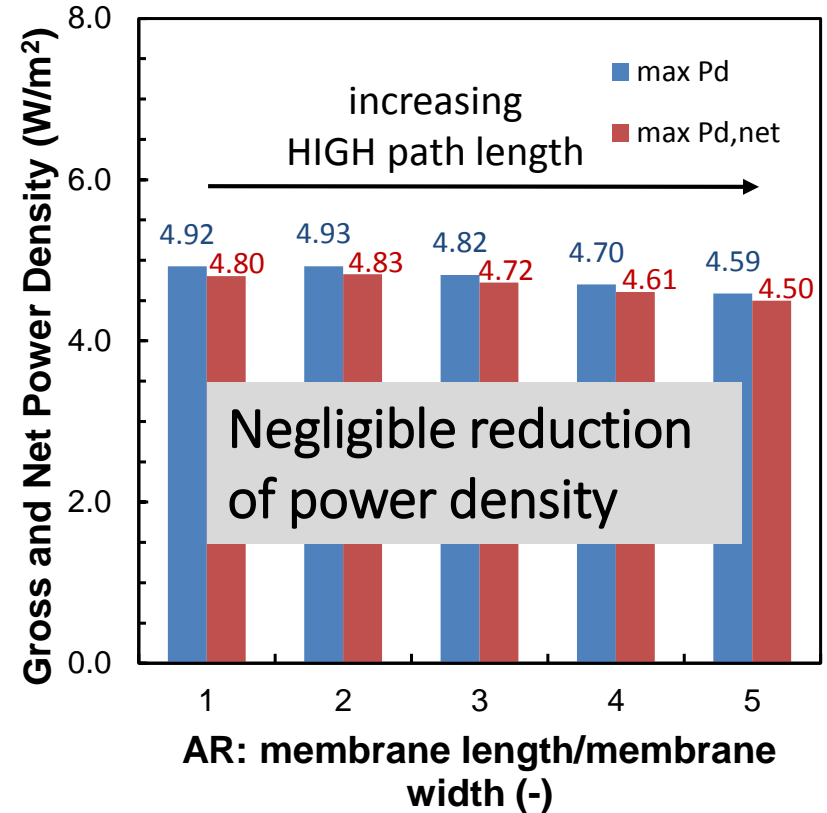
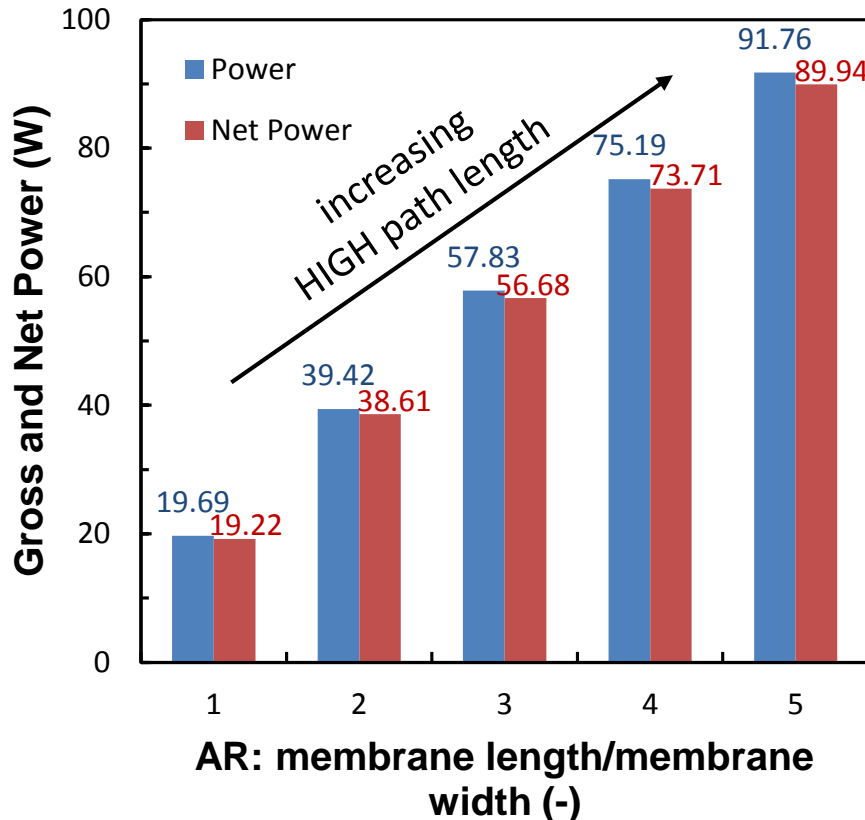
$$\text{Aspect Ratio (AR)} = \frac{\text{HIGH path length (L)}}{\text{LOW path length (b)}}$$

Aspect ratio (AR)	Membrane size (b x L)
1	20x20 
2	20x40 
3	20x60 
4	20x80 
5	20x100 



Different path length for diluate/concentrate (2/2)

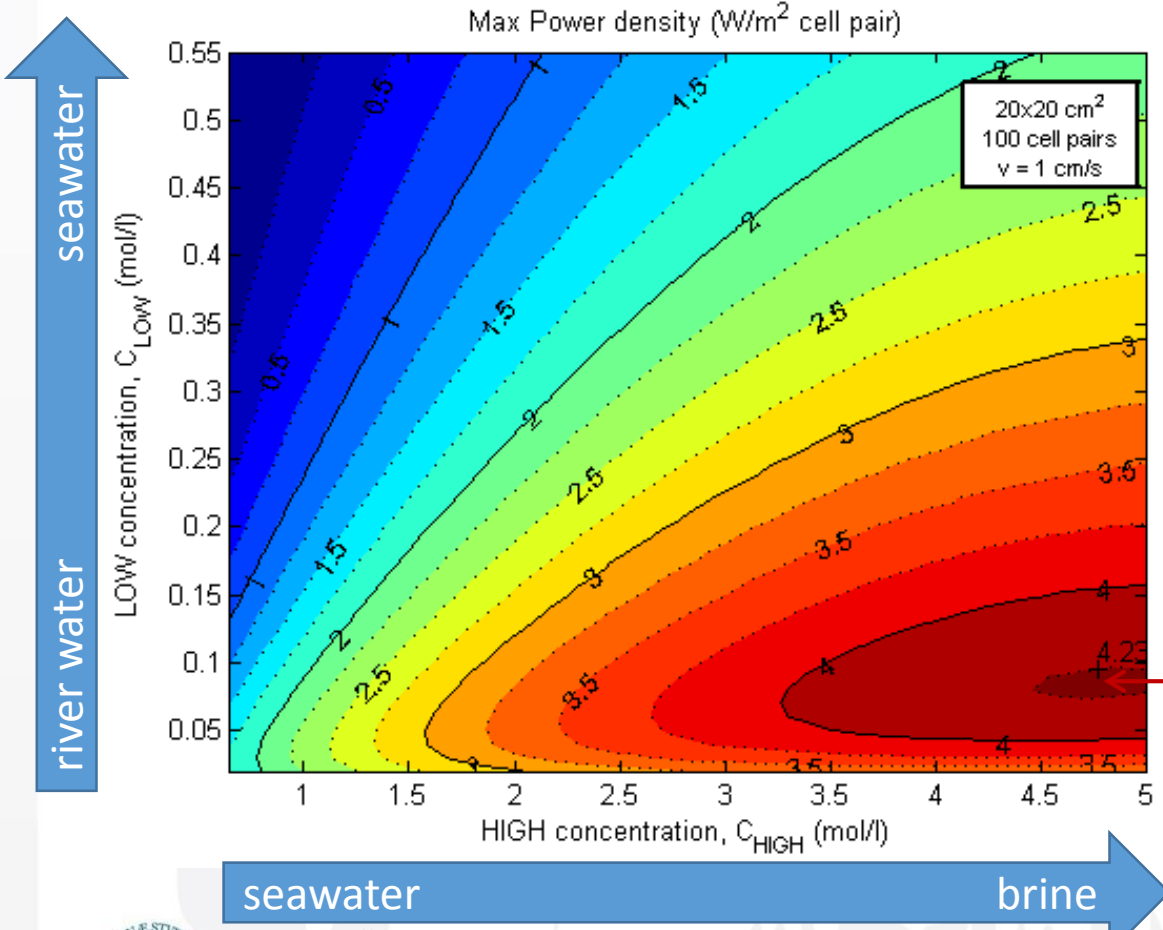
- Effect of Aspect Ratio on Power output



Simulations of a 100-cells stack equipped with Fujifilm membranes, 270 μm spacers; $C_{LOW} = 0.1 \text{ M}$; $C_{HIGH} = 5 \text{ M}$; $v_{HIGH} = v_{LOW} = 1 \text{ cm/s}$; membrane width: $b = 20 \text{ cm}$; $T=30^{\circ}\text{C}$.

Exploring the optimal operating conditions (1/3)

- Effect of salt concentration



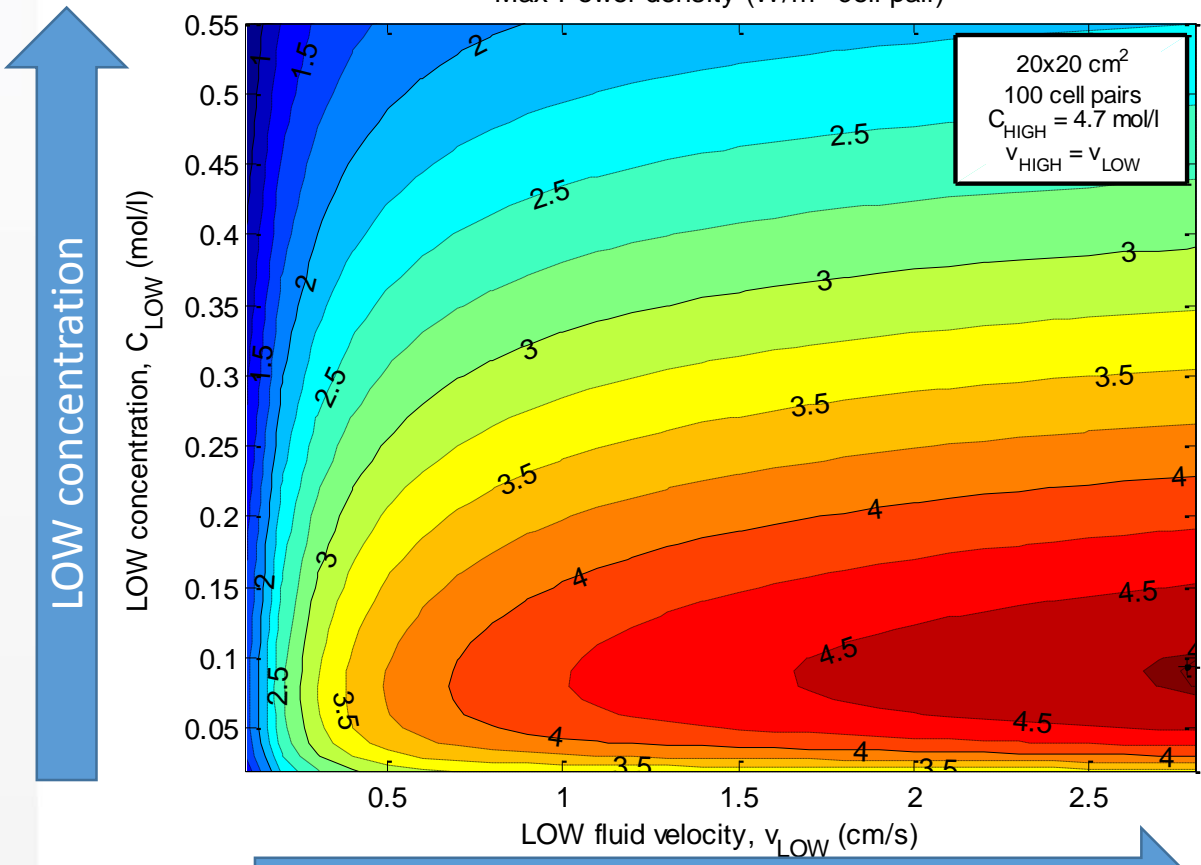
BEST conditions:
 brackish water (0.07 – 0.1 M)
 + brine (4.5 – 5 M)



Simulations of a 20x20 cm² stack (100-cells) equipped with Fujifilm membranes, 270 μm spacers; feed flow velocity: 1 cm/s; T=20°C.

Exploring the optimal operating conditions (2/3)

- Effect of concentration/flow rate for diluate



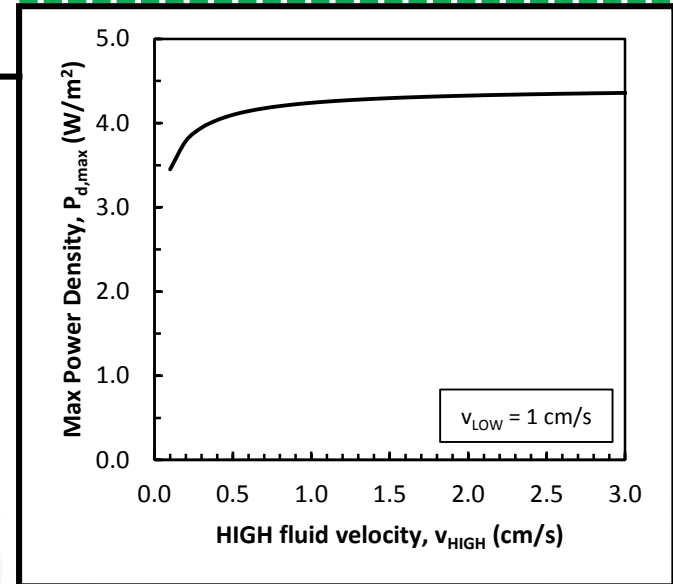
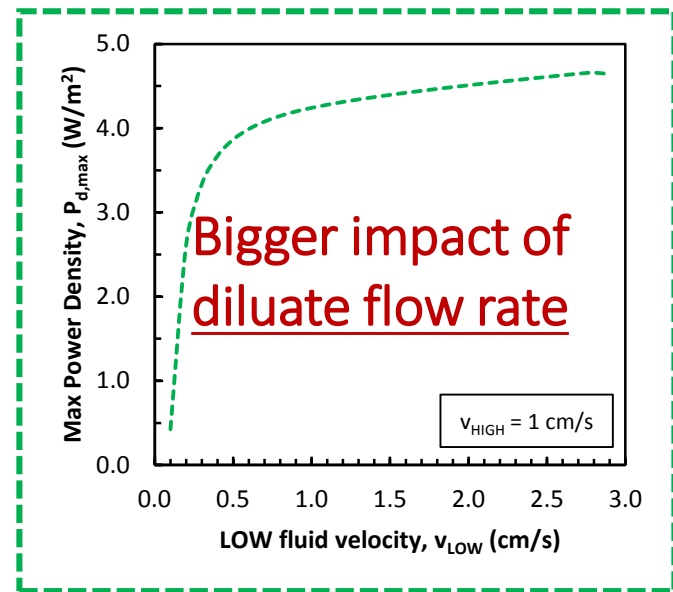
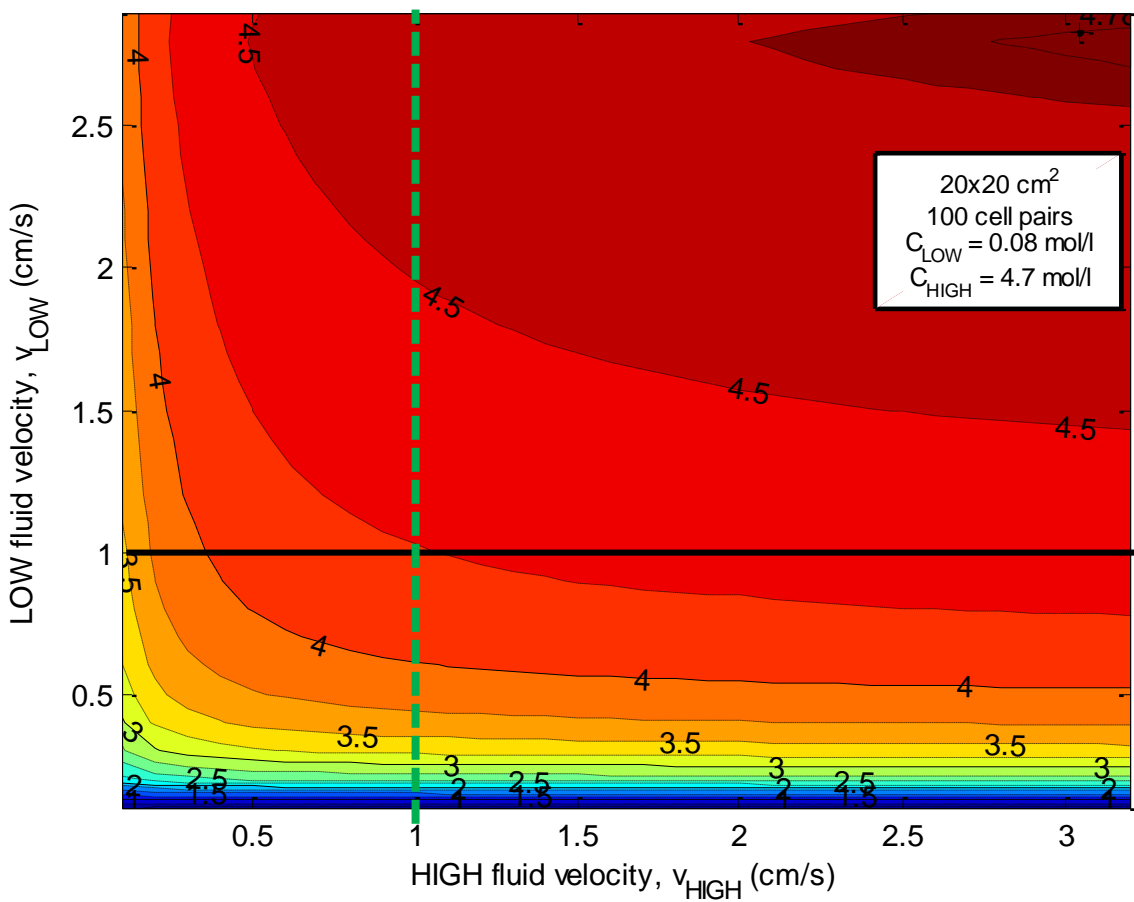
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Simulations of a 20x20 cm² stack (100-cells) equipped with Fujifilm membranes, 270 μm spacers; $C_{HIGH} = 4.7$ M; $v_{HIGH} = v_{LOW}$; $T=20^{\circ}C$.

Exploring the optimal operating conditions (3/3)

- Influence of feed flow rates







Max Power density (W/m^2 cell pair)



Simulations of a 20x20 cm² stack (100-cells) equipped with Fujifilm membranes, 270 μm spacers; C_{LOW} = 0.08 M; C_{HIGH} = 4.7 M; T=20°C.



Simulation of large-scale pilot (1/2)

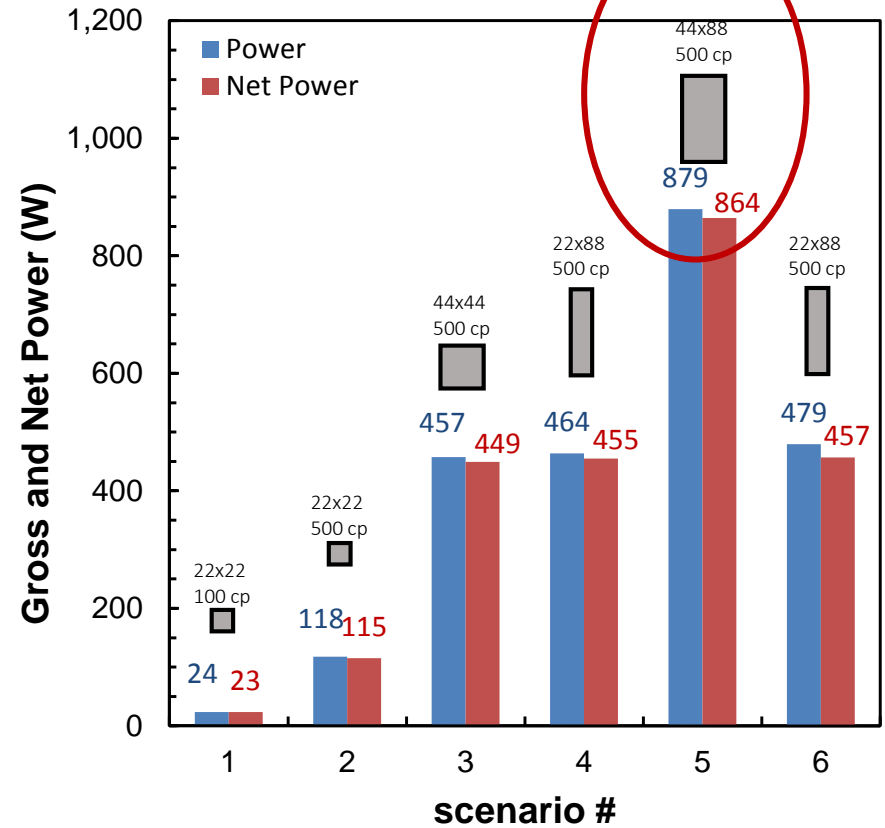
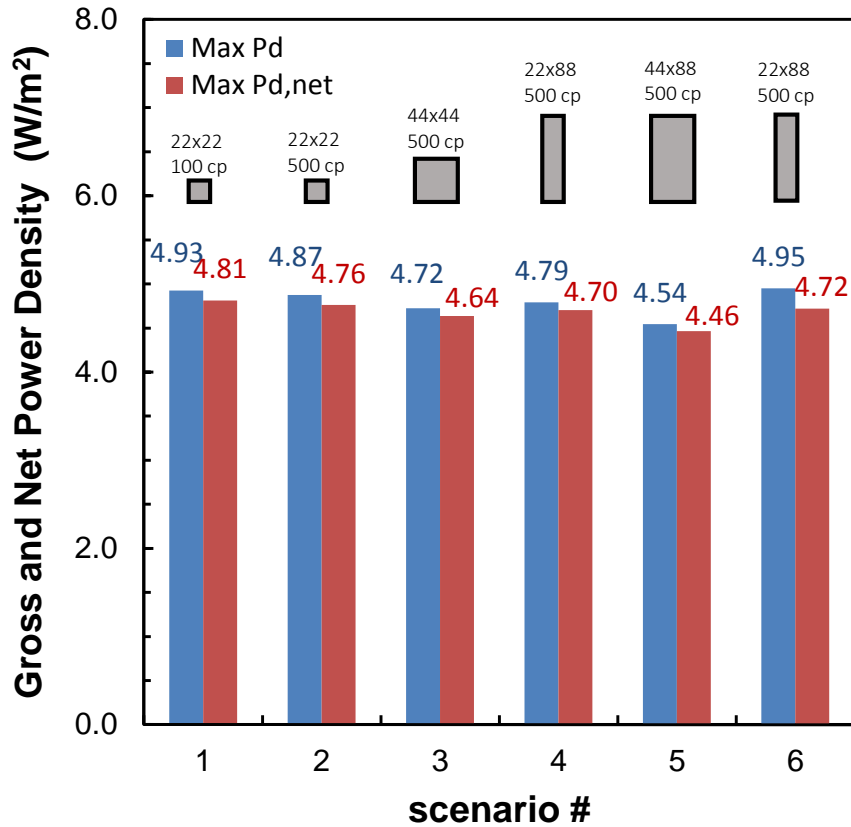
Scenario #	Stack size (cm)	cell pair Area	N° cell pairs	Notes
1	22 x 22 	0.05 m ²	100	Reference case (small prototype)
2	22 x 22 	0.05 m ²	500	Larger number of cell pairs
3	44 x 44 	0.20 m ²	500	symmetrical stack
4	22 x 88 	0.20 m ²	500	asymmetrical stack, AR = 4
5	44 x 88 	0.44 m ²	500	asymmetrical stack, AR = 2
6	22 x 88 	0.20 m ²	500	asymmetrical stack, different velocity (v _{LOW} = 1 cm/s, v _{HIGH} = 2 cm/s)

Overall conditions:

- HIGH concentration: 5 M NaCl
- LOW concentration: 0.1 M NaCl
- Temperature : 30°C
- Fluid velocity: 1 cm/s (except for scenario # 6)

Simulation of large-scale pilot (2/2)

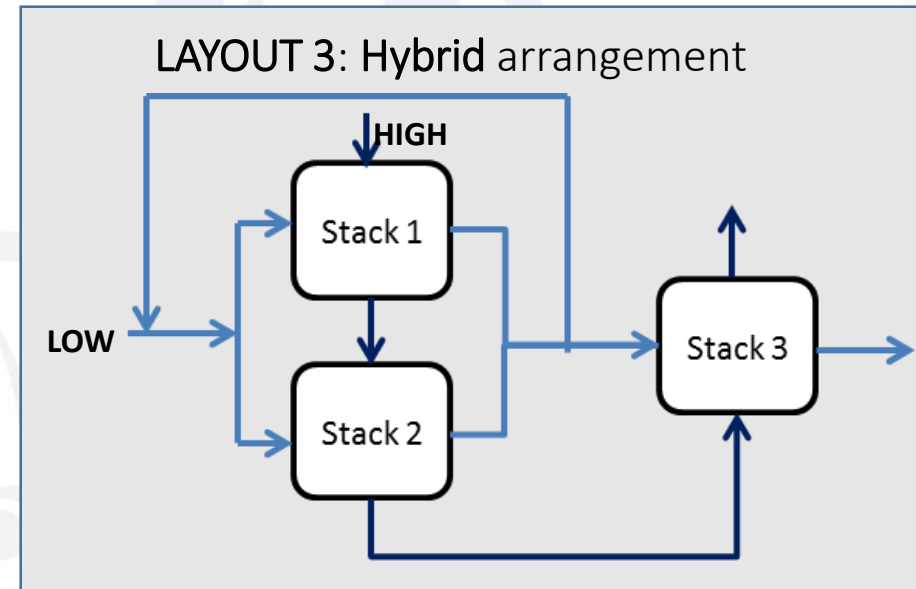
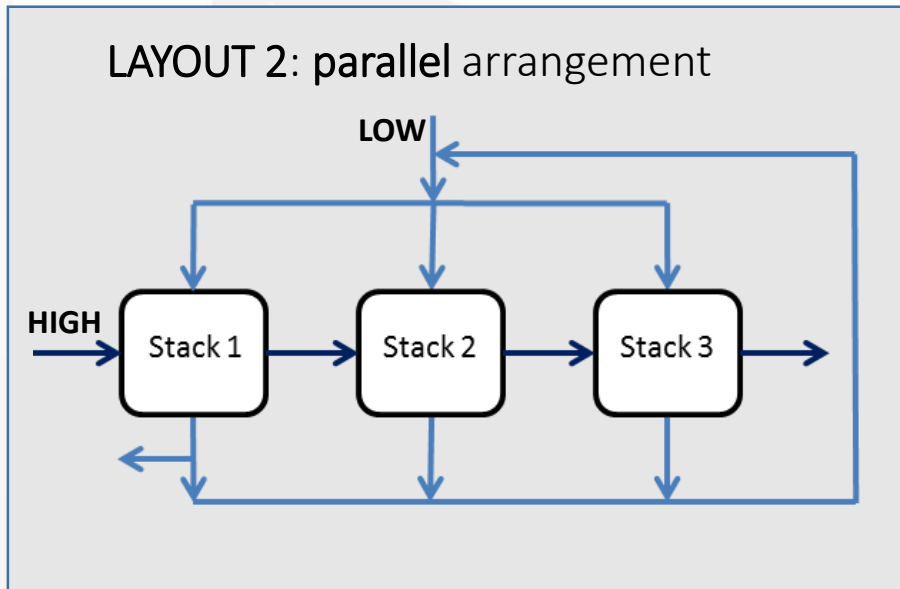
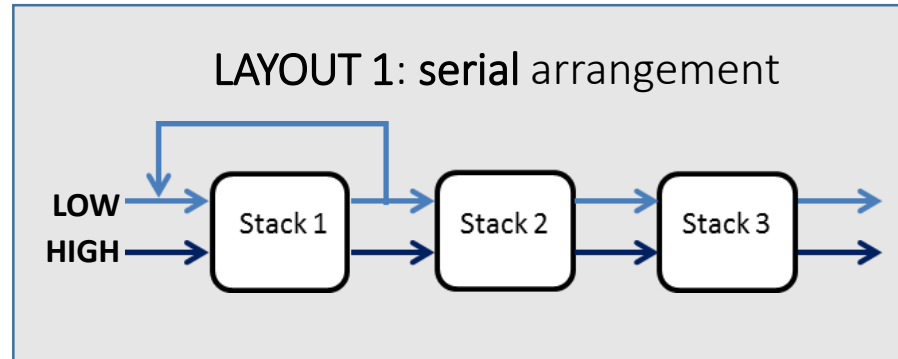
- Gross and Net Power density



Simulations of stacks equipped with Fujifilm membranes, 270 μm spacers;
 $C_{LOW} = 0.1 M$; $C_{HIGH} = 5 M$; $T=30^{\circ}C$.

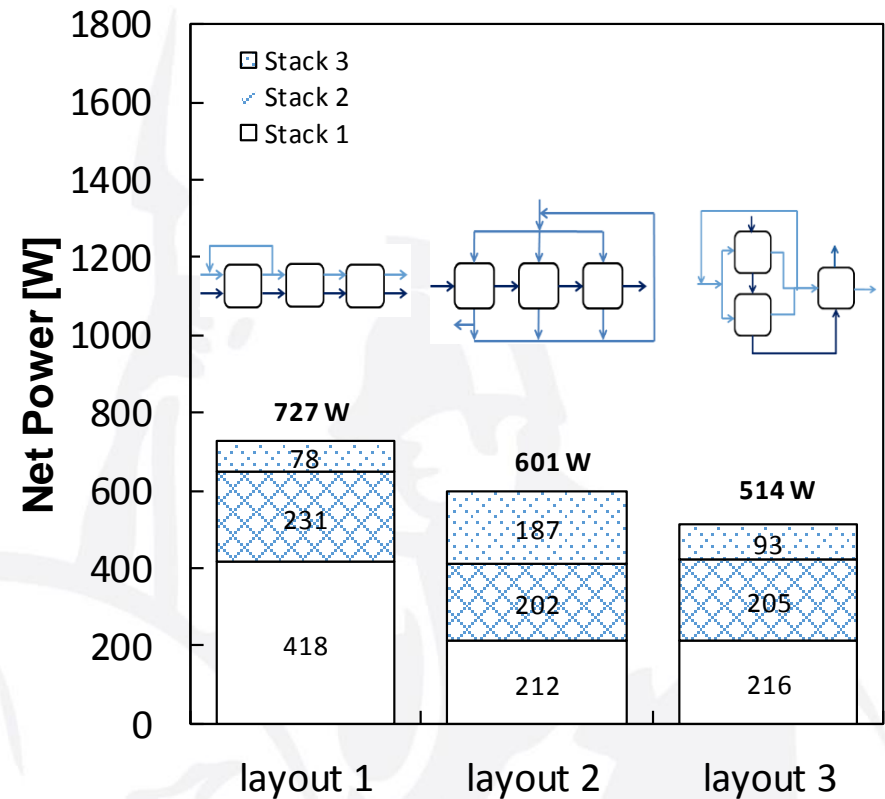
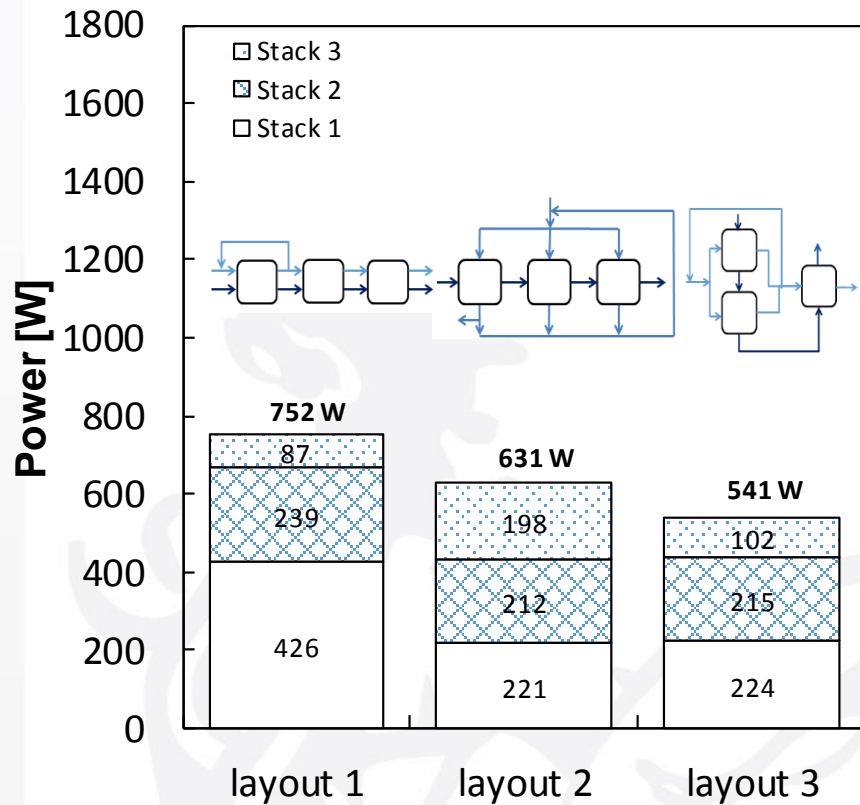
Process simulation for a 3 RED units plant (1/4)

- Investigated layouts



Process simulation for a 3 RED units plant (2/4)

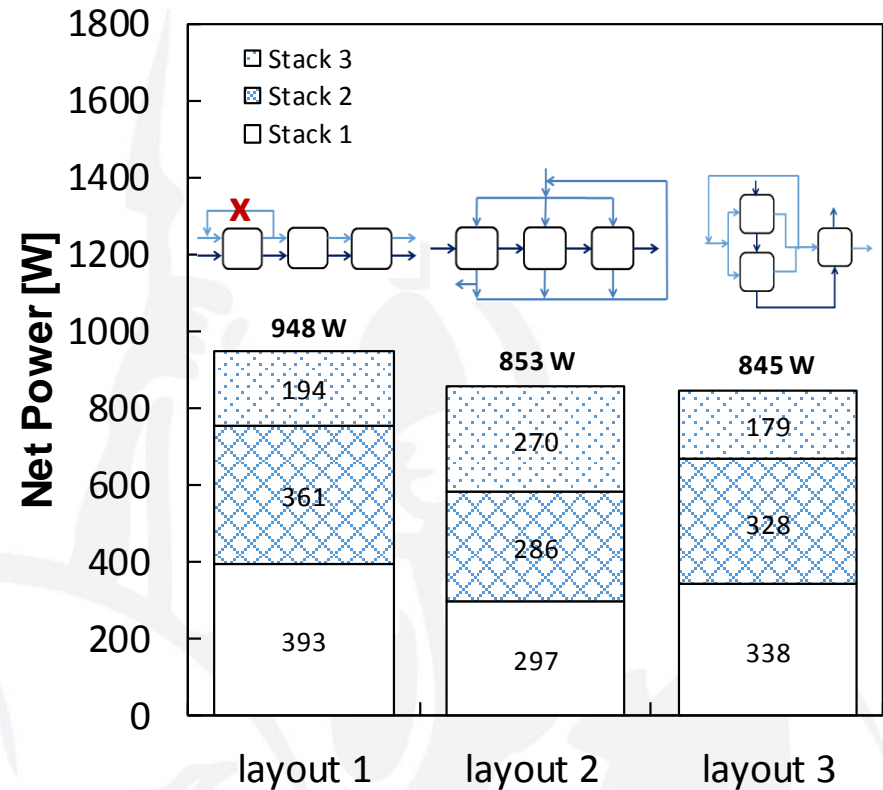
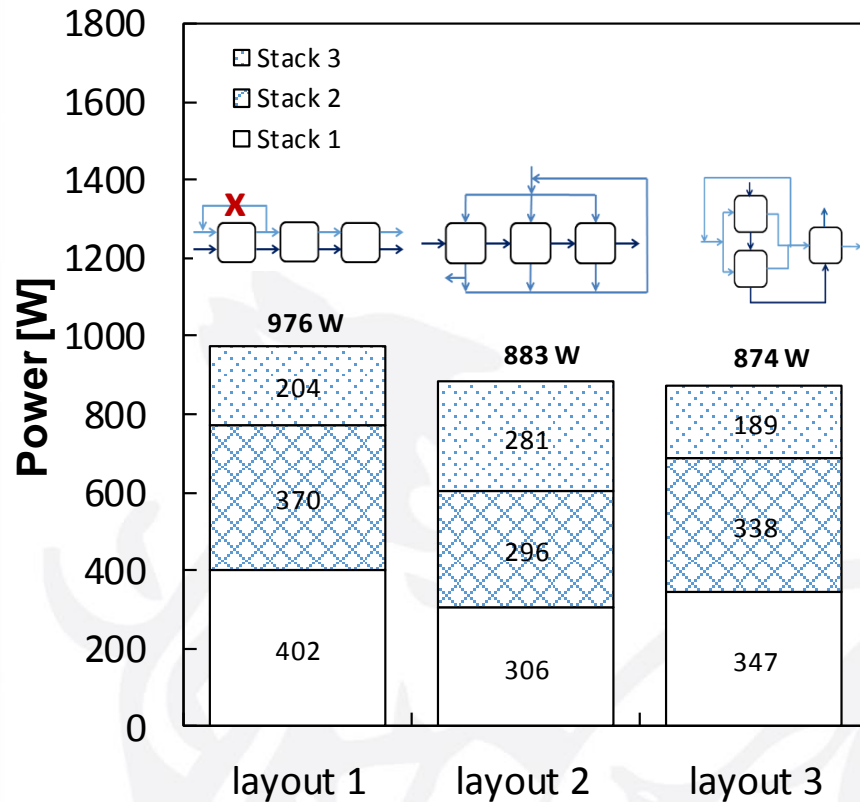
- Inlet diluate flow rate: 20 l/min



3 stacks (500 cells) equipped with Fujifilm membranes 44×44 cm, 270 μm woven spacers.
 $C_{\text{HIGH}} = 5\text{M}$; $Q_{\text{HIGH}} = 29.4\text{ lt/min}$; make-up of brackish water, $Q_{\text{MU}} = 20\text{ lt/min}$, $C_{\text{MU}} = 0.03\text{M}$

Process simulation for a 3 RED units plant (3/4)

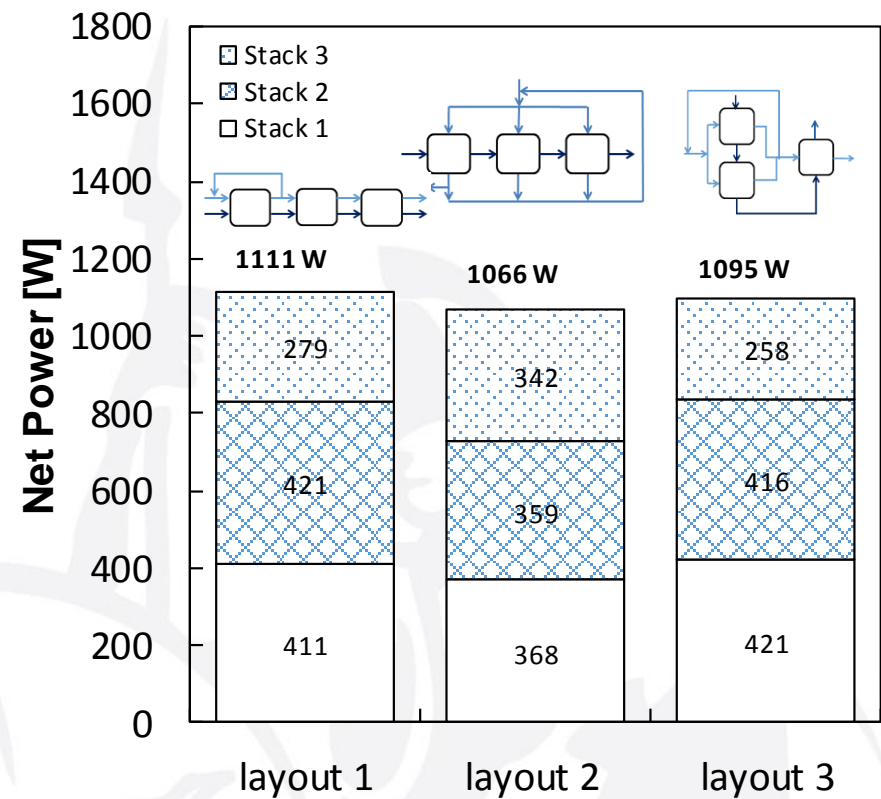
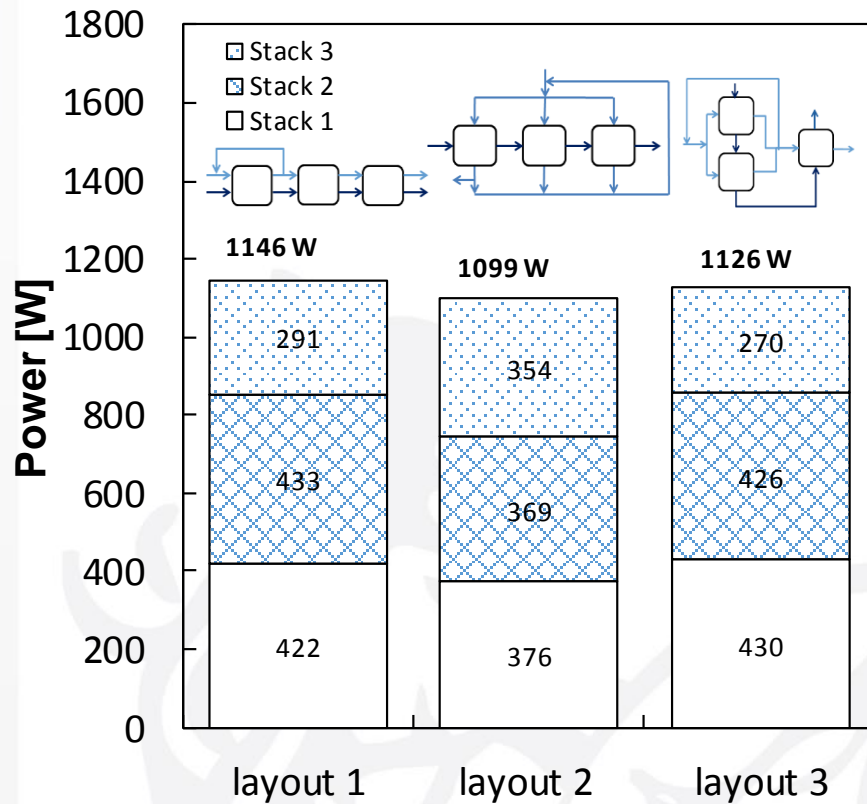
- Inlet diluate flow rate: 29.4 l/min



3 stacks (500 cells) equipped with Fujifilm membranes 44×44 cm and 270 μm woven spacers.
 $C_{\text{HIGH}} = 5\text{M}$; $Q_{\text{HIGH}} = 29.4 \text{ lt/min}$; make-up of brackish water, $Q_{\text{MU}} = 29.4 \text{ lt/min}$, $C_{\text{MU}} = 0.03\text{M}$.

Process simulation for a 3 RED units plant (4/4)

- Inlet diluate flow rate: **40 l/min**



3 stacks (500 cells) equipped with Fujifilm membranes 44×44 cm and 270 μm woven spacers.
 $C_{\text{HIGH}} = 5\text{M}$; $Q_{\text{HIGH}} = 29.4\text{ lt/min}$; make-up of brackish water, $Q_{\text{MU}} = 40\text{ lt/min}$, $C_{\text{MU}} = 0.03\text{M}$.

Conclusions

- ✓ A **Simulator for RED process** was developed
- ✓ Asymmetrical stack design (i.e. longer path for concentrate) increases process performance
- ✓ **brackish water flow rate/concentration** are key parameters for the process
- ✓ **Power output >1 kW** can be reached using 3 RED units (44x44 cm², 500 cell pairs)

Acknowledgments



www.reapower.eu

Project title: *Reverse Electrodialysis Alternative Power Production*

Call identifier: FP7-ENERGY-2010-FET

(Future Emerging Technologies for Energy Applications)

The Future

of sustainable energy production

Next events on Salinity Gradient Power

INES Events

- 10-11 June 2014 Montreal (Canada)
- 23 June 2014 Brussels (Belgium)

CAPMIX Conference

- 10-12 September 2014 Leeuwarden (The Netherlands)

*Thank you
for your attention*



**EuroMed 2015
Desalination for Clean Water and Energy
Palermo, Italy, 10-14 May 2015**



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