



UNIVERSITÀ
DEGLI STUDI
DI PALERMO

Dipartimento di Ingegneria Chimica,
Gestionale, Informatica, Meccanica (DICGIM)



Ion Exchange Membranes for Salinity Gradient Power production from brines: the REAPower project

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The REAPower Project

Main facts:

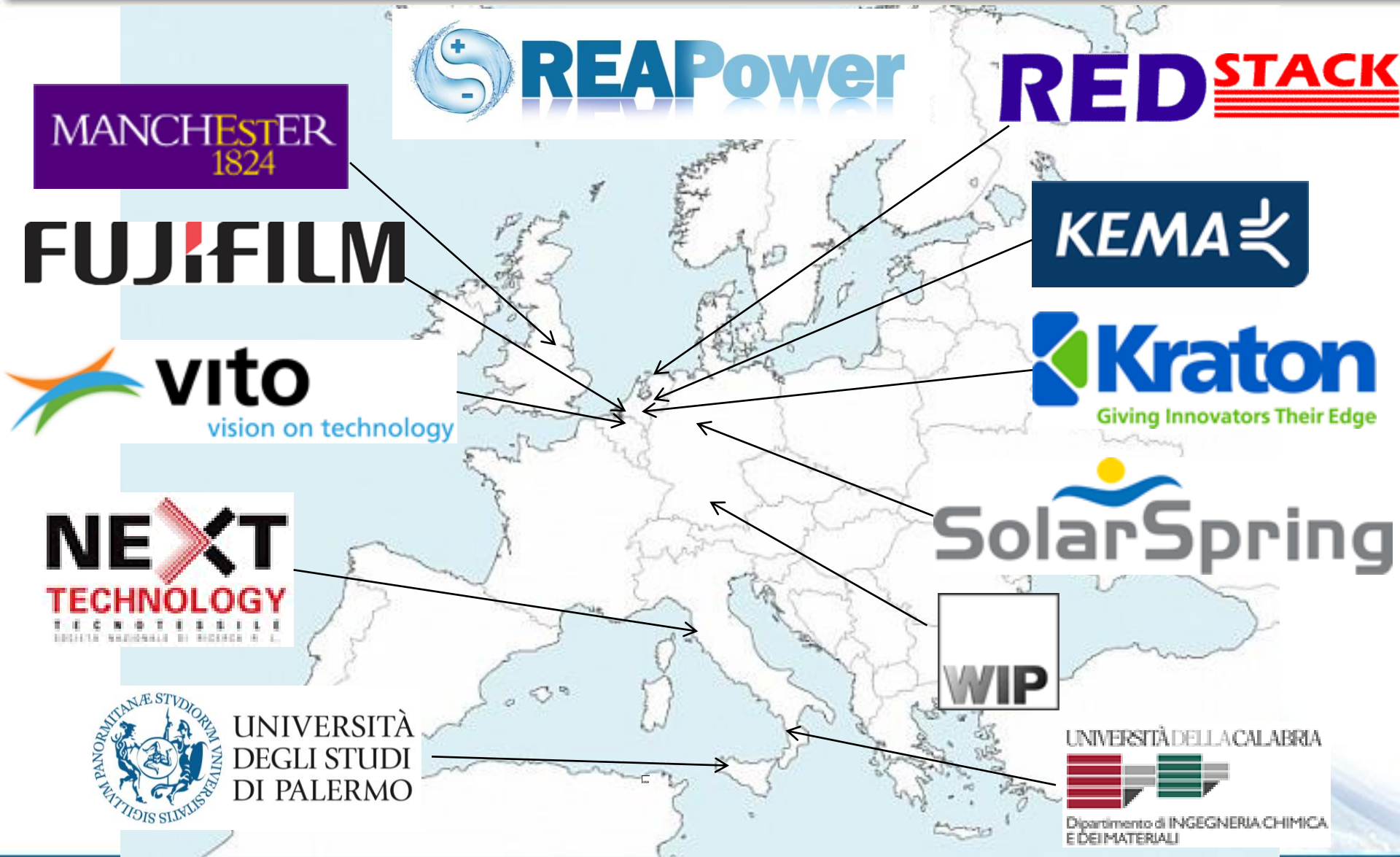


- Project acronym: “Reverse Electrodialysis for Alternative Power production”
- Cooperative project financed through the FP7 programme
- Starting date: 1 October 2010
- Closing date: 30 September 2014

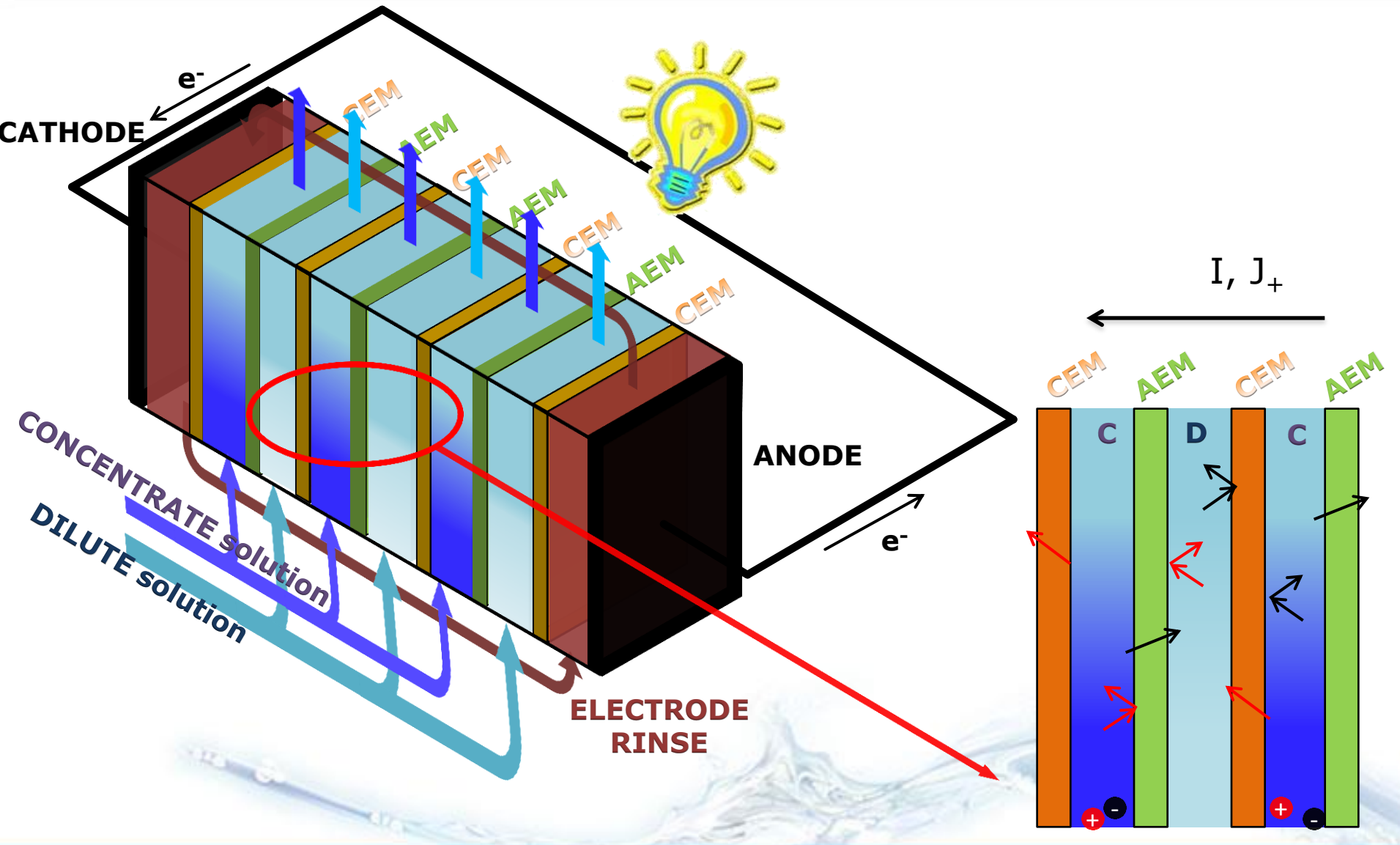
The Future

of sustainable energy production

The REAPower Project Consortium



The Reverse Electrodialysis technology



The REAPower Project

The idea...

to produce **energy from salinity gradients** generated by **sea/brackish water and ultra-concentrated brines**



Technological benefits for the SGP-RE process

new potentials for the exploitation of brines



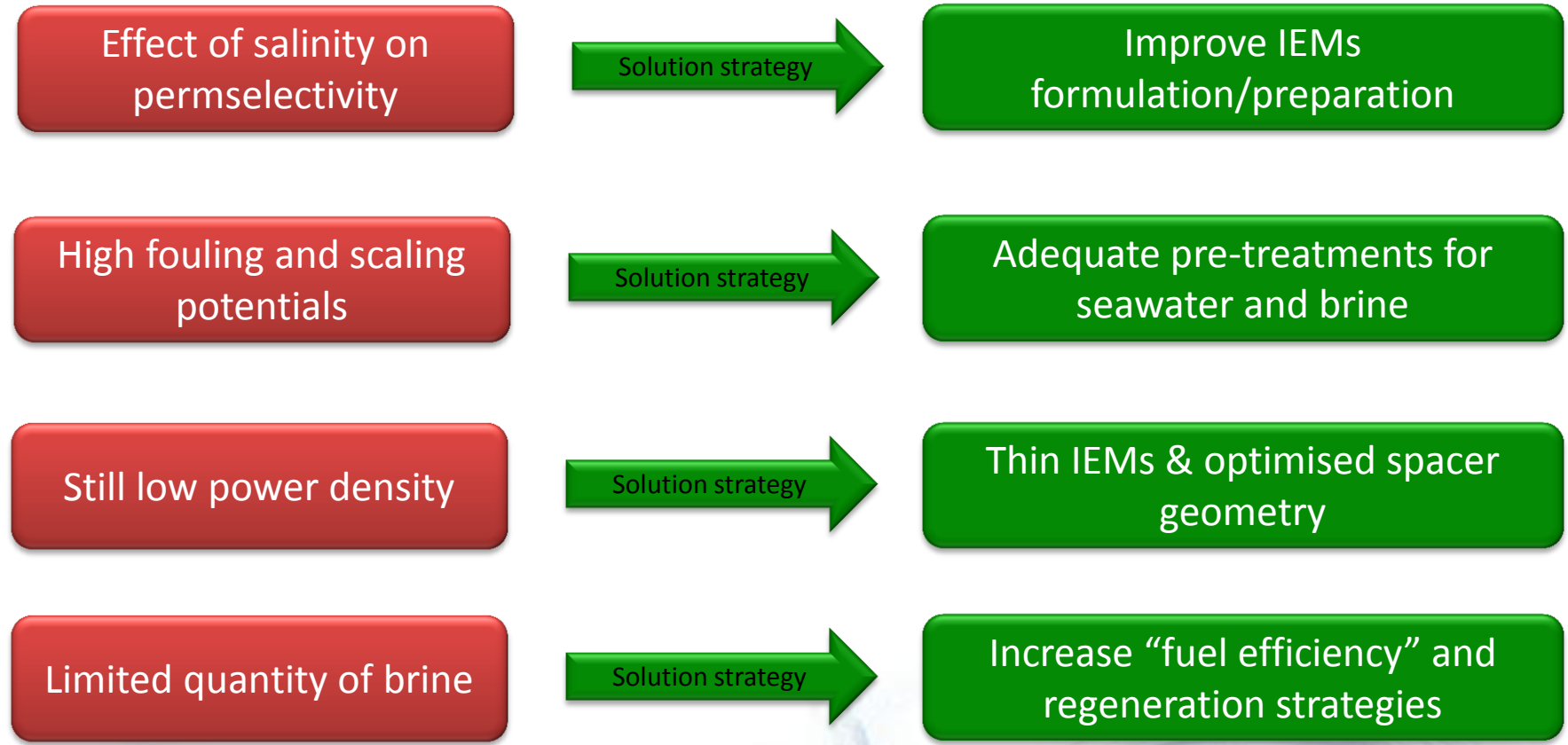
The REAPower Project

Technological basic concepts . . .

- i) Seawater ($\approx 30\text{-}35$ g/l) in the LOW conc. compartment and concentrated brine (≈ 300 g/l) in the HIGH conc. compartment dramatically reduce the electrical resistance in all battery compartments
- ii) As a result: an ultra-low overall internal resistance within the SGP-RE battery cell-pairs can be achieved . . . especially with the introduction of thinner membranes
- iii) Thus, the ultra-low internal resistance will significantly promote a higher power density of the SGP-RE battery.

The REAPower Project

Technological barriers. . .

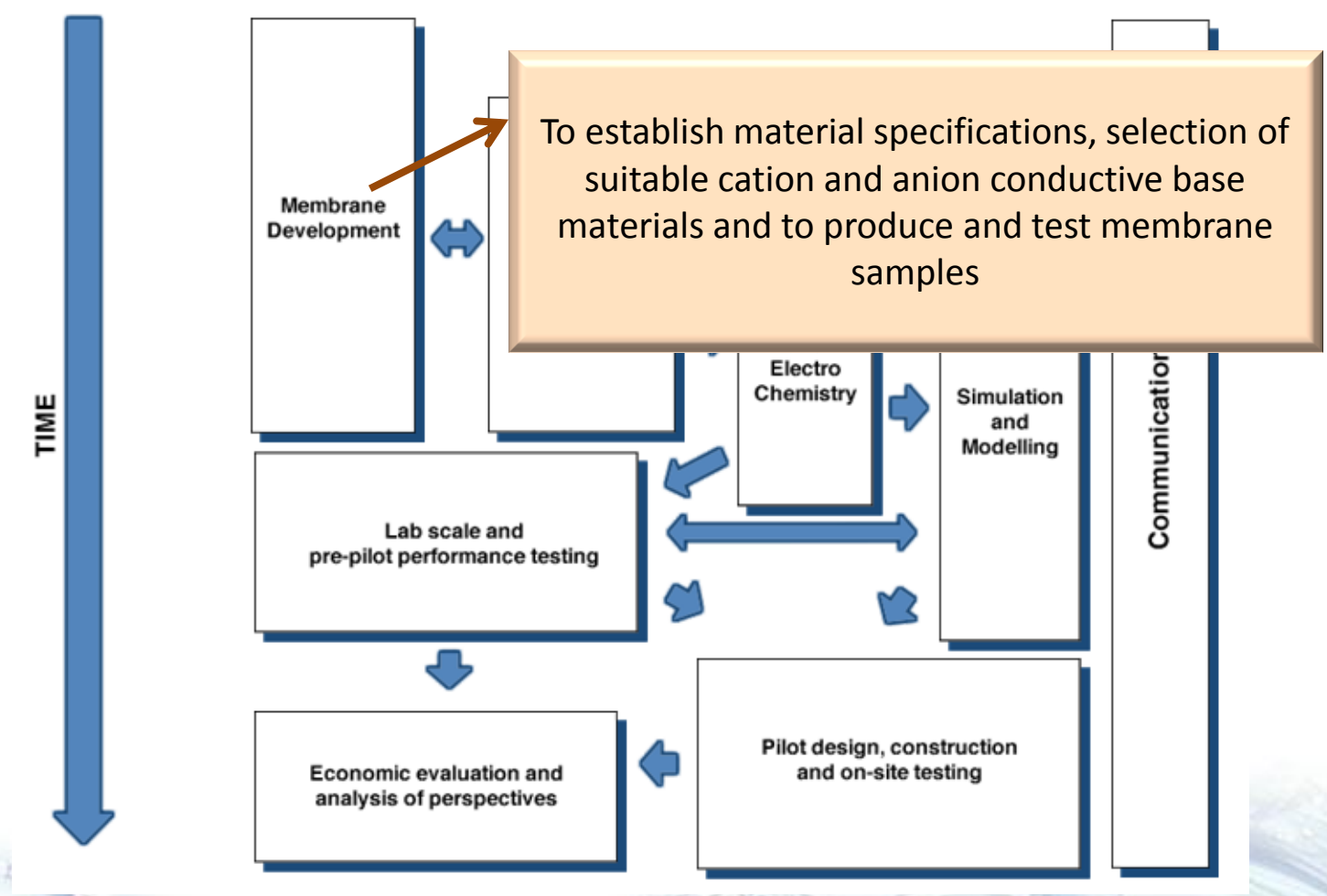


The REAPower Project

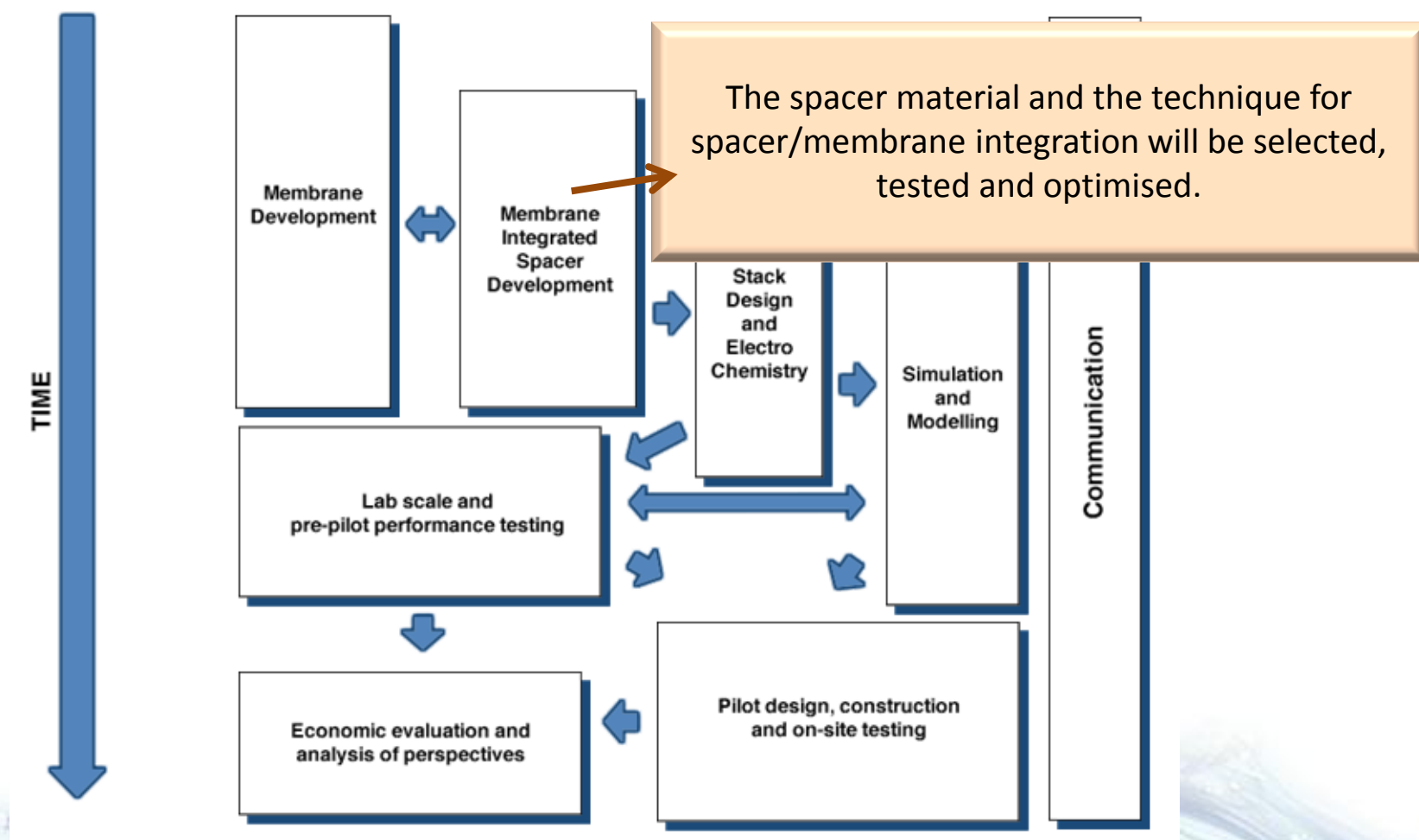
The Objectives...

- 1 • Define and optimise materials and components tailored to the requirements of the technology
- 2 • Optimise the design of the SGP-RE cell pairs and stack using computer modelling tools;
- 3 • Validate the model and assess the developed materials, components and design by laboratory stack tests;
- 4 • Evaluate and improve the system performance through tests on a prototype fed with real brine;
- 5 • Analyse the “economics” and assess the perspectives
- 6 • Define the next R&D steps

WP2. Membrane Development



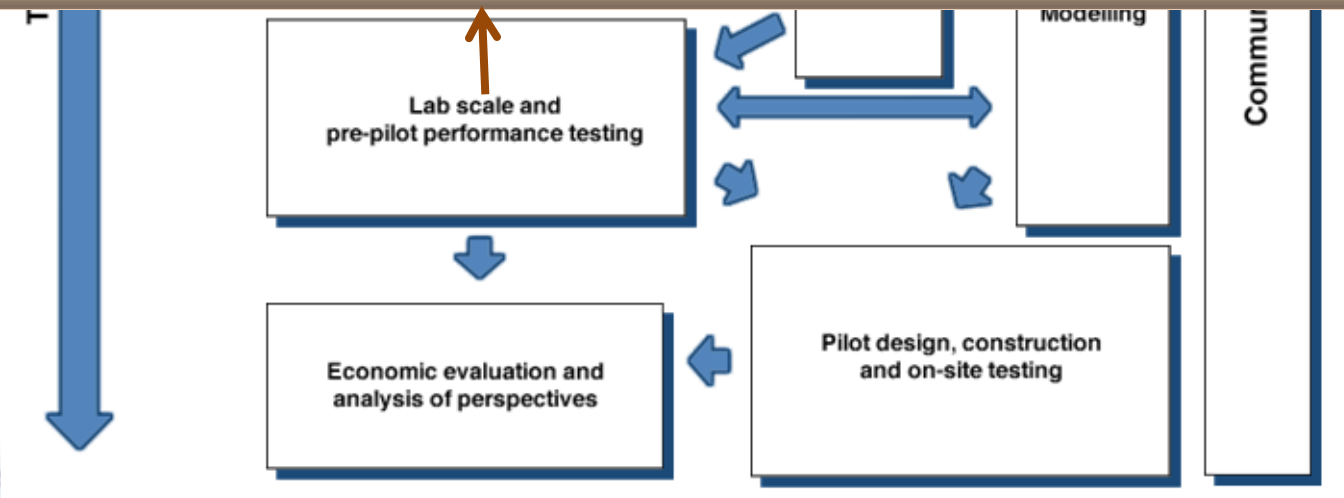
WP3. Membrane Integrated Spacer Development



WP6. Lab-scale performance testing

Extensive testing of the laboratory stack in order to evaluate the effect of the hydraulic conditions and to study the effect of the real feed composition on the process.

The combination of this technology with a membrane distillation concept and the pre-treatment requirements of different brine inputs will be assessed.



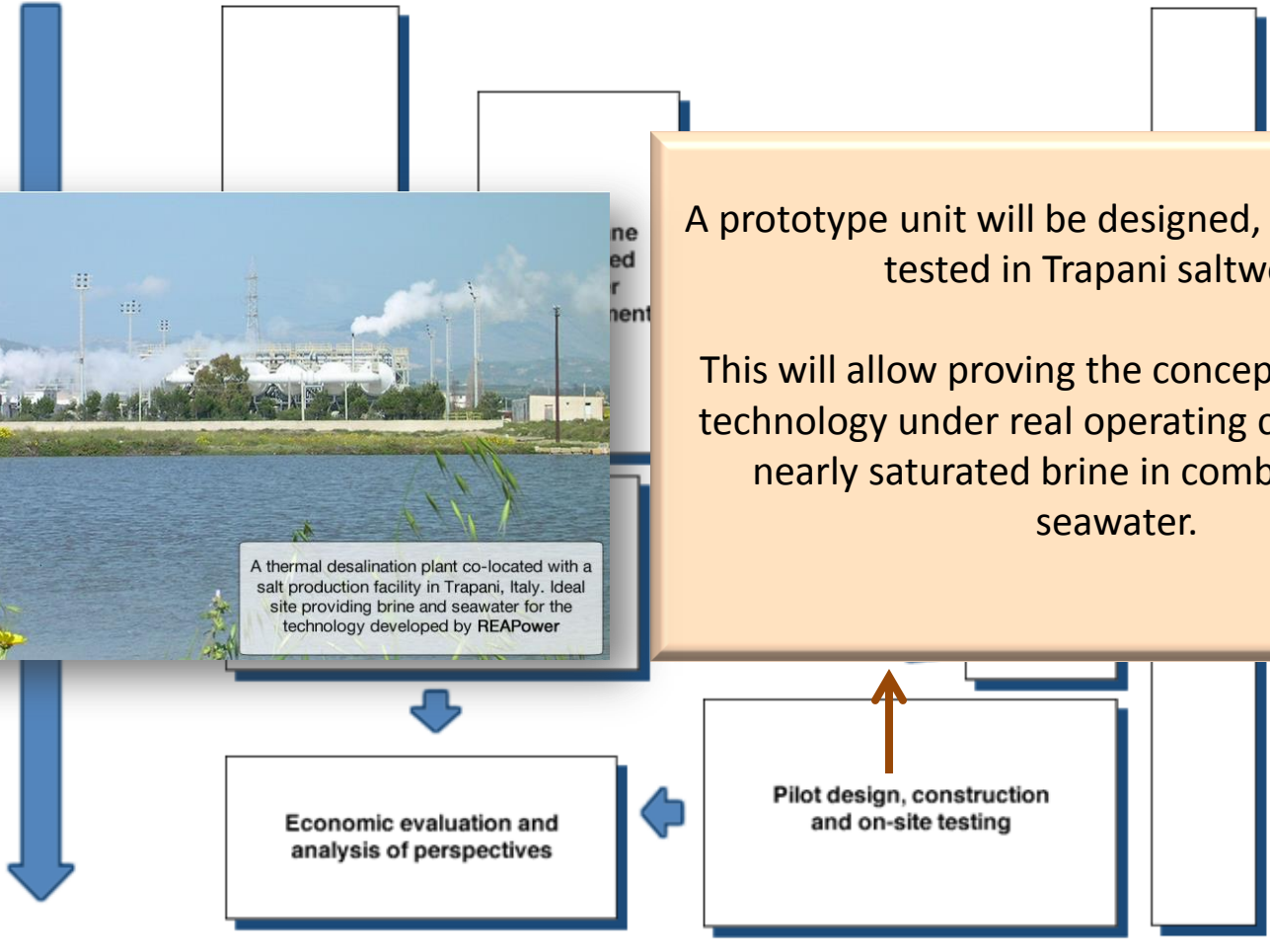
WP7. Design, construction, testing of the prototype



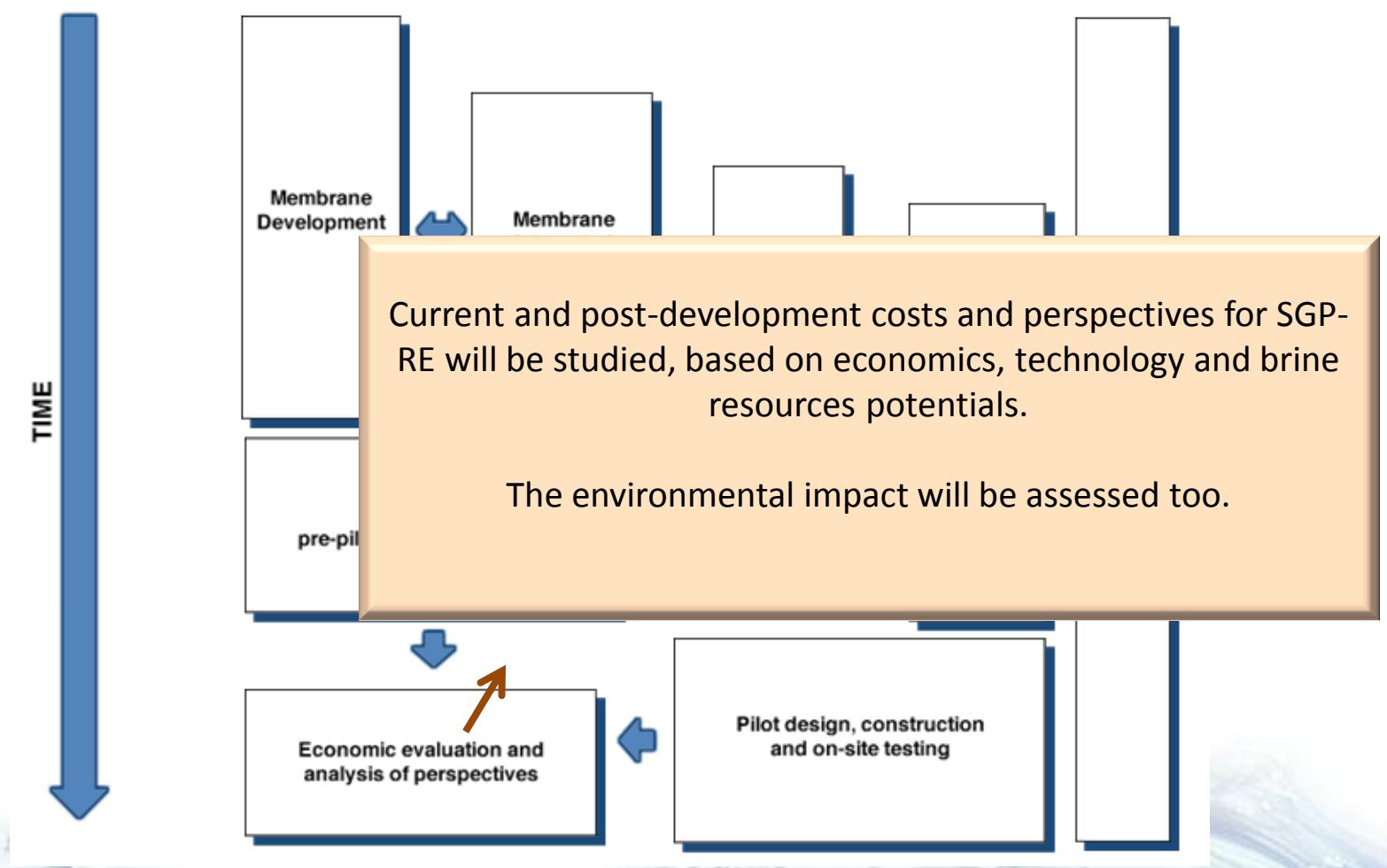
A thermal desalination plant co-located with a salt production facility in Trapani, Italy. Ideal site providing brine and seawater for the technology developed by REAPower

A prototype unit will be designed, constructed and tested in Trapani saltworks.

This will allow proving the concept of the SGP-RE technology under real operating conditions using nearly saturated brine in combination with seawater.



WP8. Economic evaluation/analysis of perspectives



Membranes performance enhancements

Increased permselectivity



Permselectivity has achieved values between 65 and 90% when in contact with almost saturated brine

Reduced membrane resistance



Membrane specific resistance has been reduced to values around 1.5-2.5 $\Omega \cdot \text{cm}^2$ aiming at a 3-5 folds reduction in the next months



Redox couples and stack design

Redox couples selection



Several redox couples have been tested under different conditions, finding the most promising for the SGP-RE prototype:
 $\text{FeCl}_3/\text{FeCl}_2$; $\text{Water}/\text{Na}_2\text{SO}_4$;
 $[\text{Fe}(\text{CN})_6]^{3-}/[\text{Fe}(\text{CN})_6]^{4-}$

2 stack generations already designed and tested



Two different stack geometries have been already designed, constructed and tested and are now available for the consortium

IEM-integrated Spacer & Fluid Dynamics optimisation

Membrane Integrated Spacer

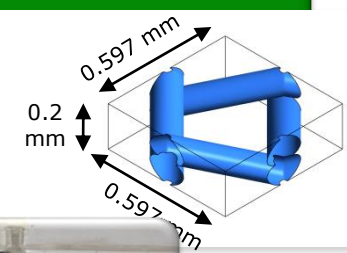
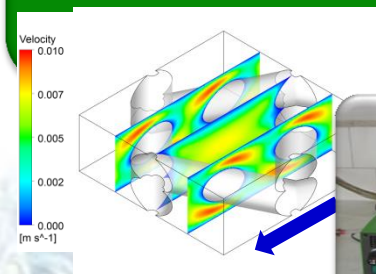


Tests are being performed for the preparation of Membrane Integrated Spacers, aiming at membrane thickness in the range 10-20 μm

Choice of spacer thickness and geometry

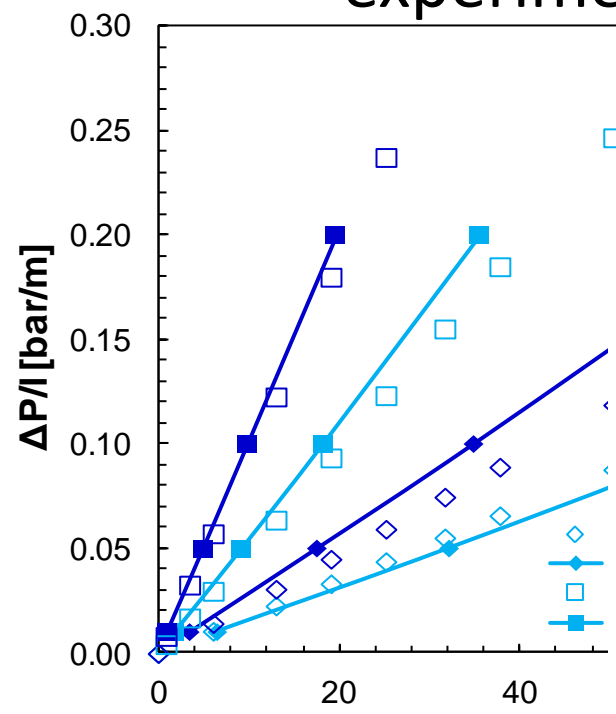


CFD simulations have been carried out along with experimental characterisation of different spacer and geometries

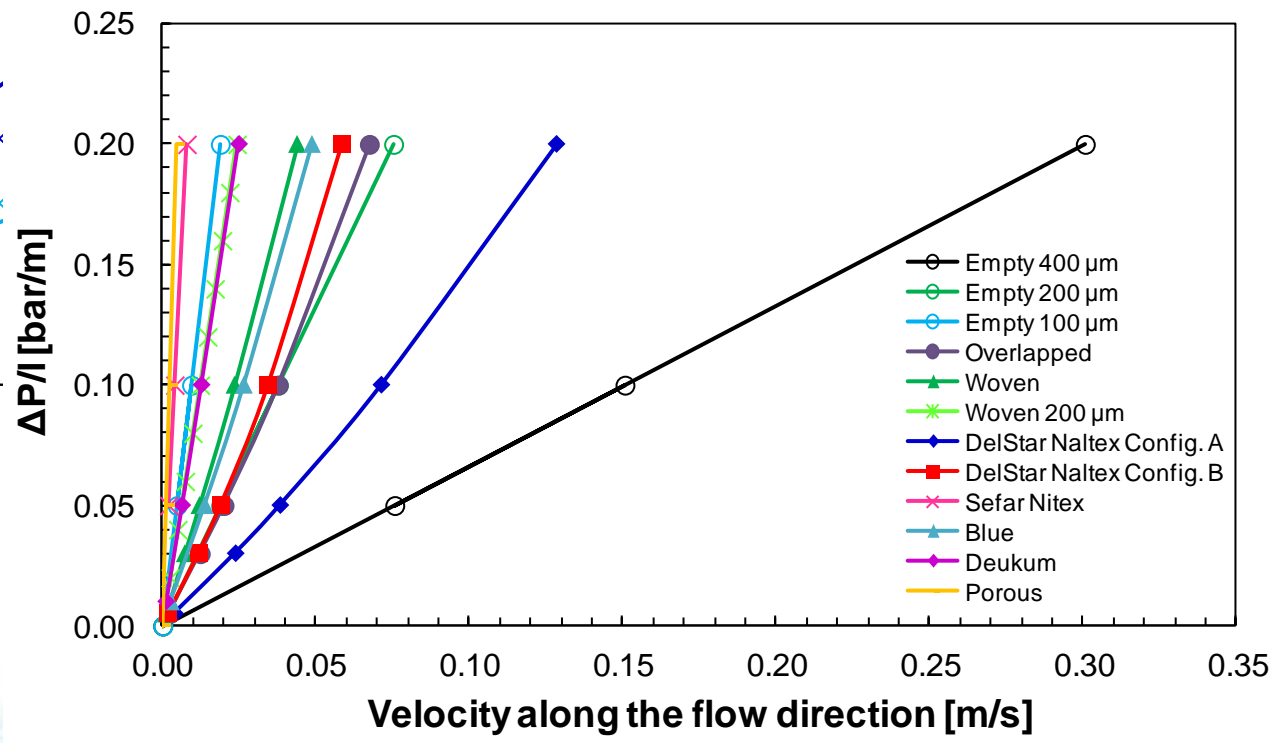


CFD Modelling: prediction of pressure drops

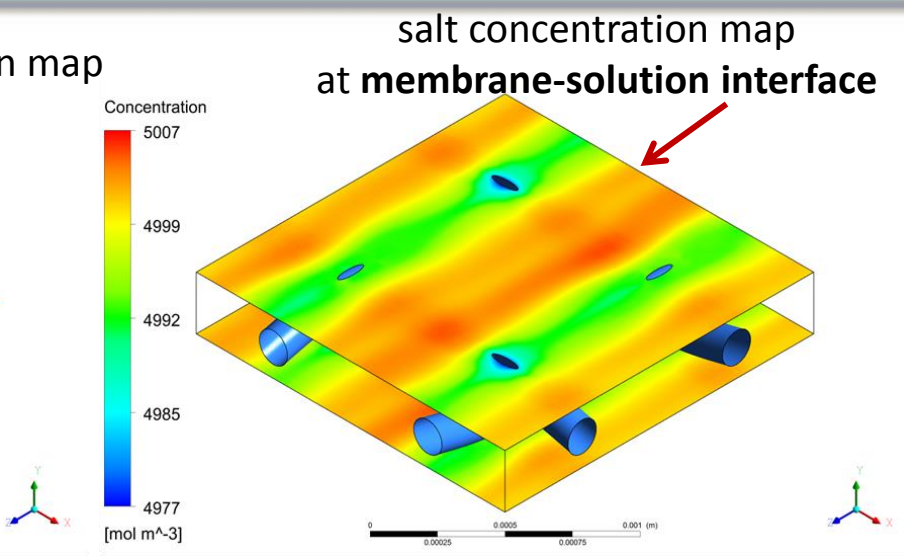
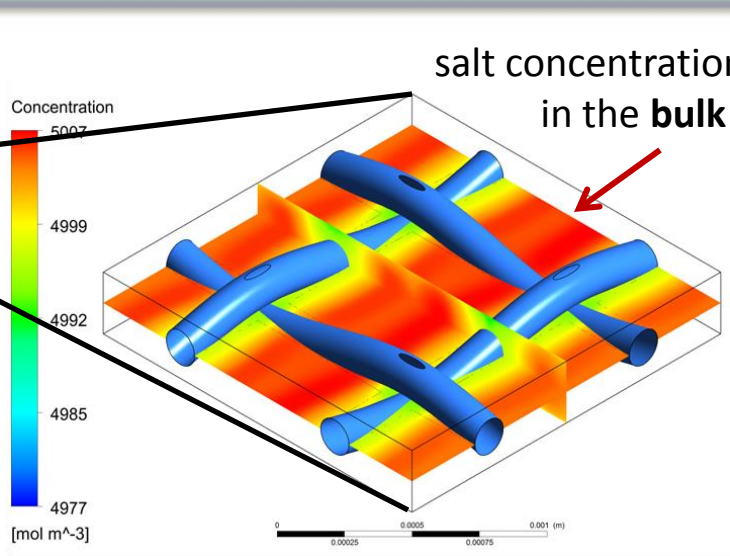
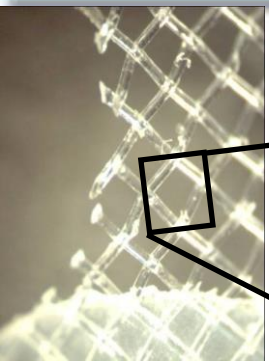
Model validation with experimental results



Simulations with different commercial spacers

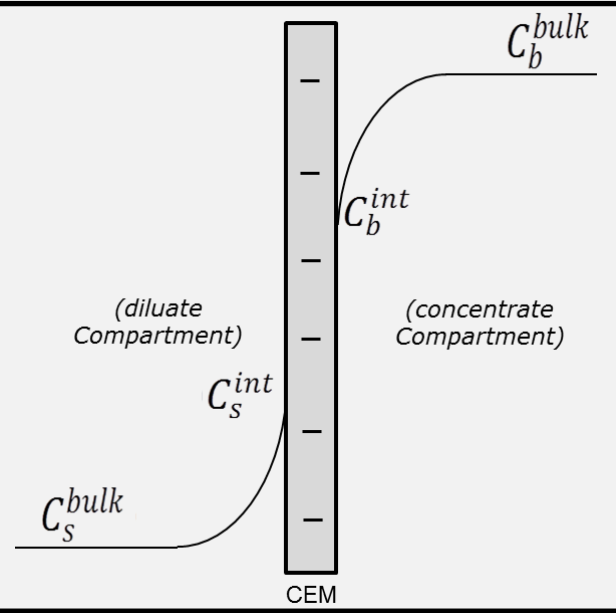


CFD Modelling: prediction of polarisation phenomena



Polarisation Coefficients:

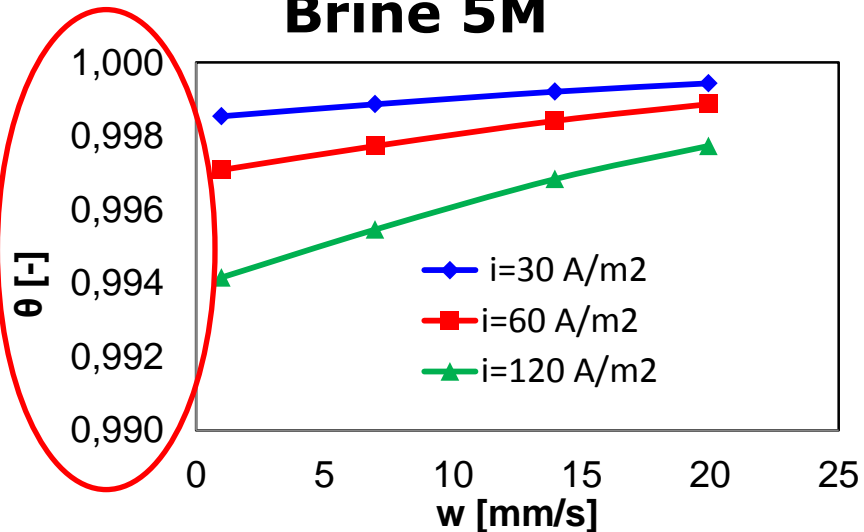
$$\left\{ \begin{aligned} \vartheta_b &= \frac{C_b^{int}}{C_b^{bulk}} \\ \vartheta_s &= \frac{C_s^{bulk}}{C_s^{int}} \end{aligned} \right.$$



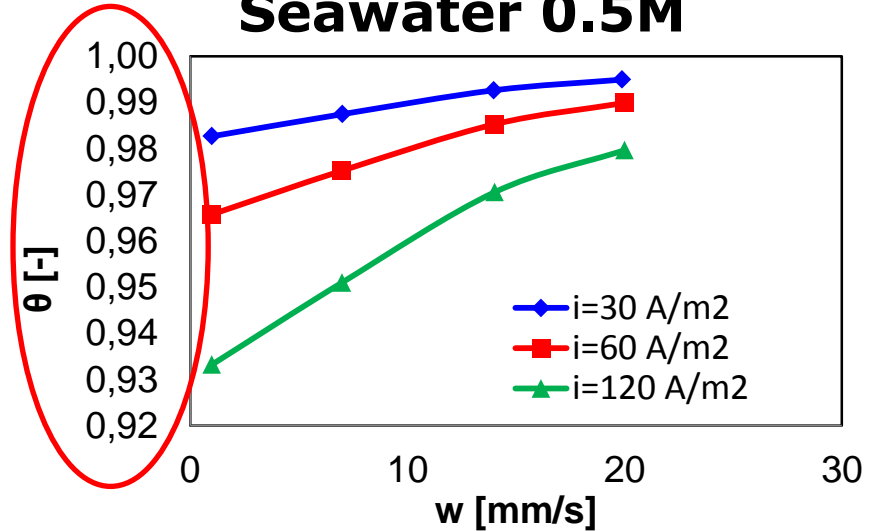
CFD Modelling: prediction of polarisation phenomena

Polarization factor for Deukum spacer-filled channels

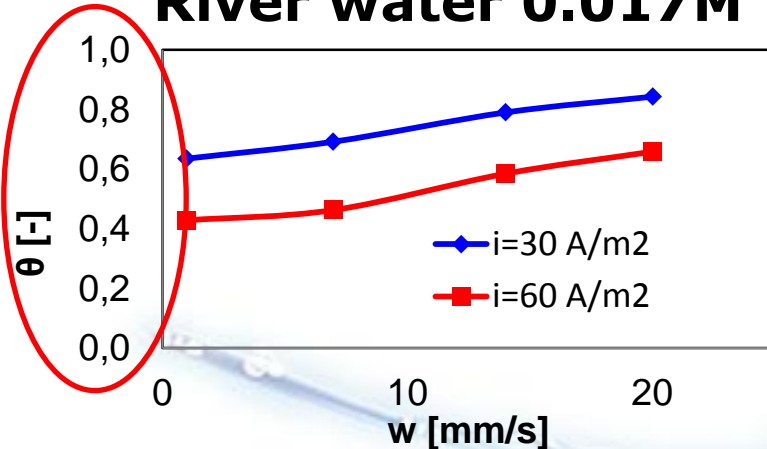
Brine 5M



Seawater 0.5M



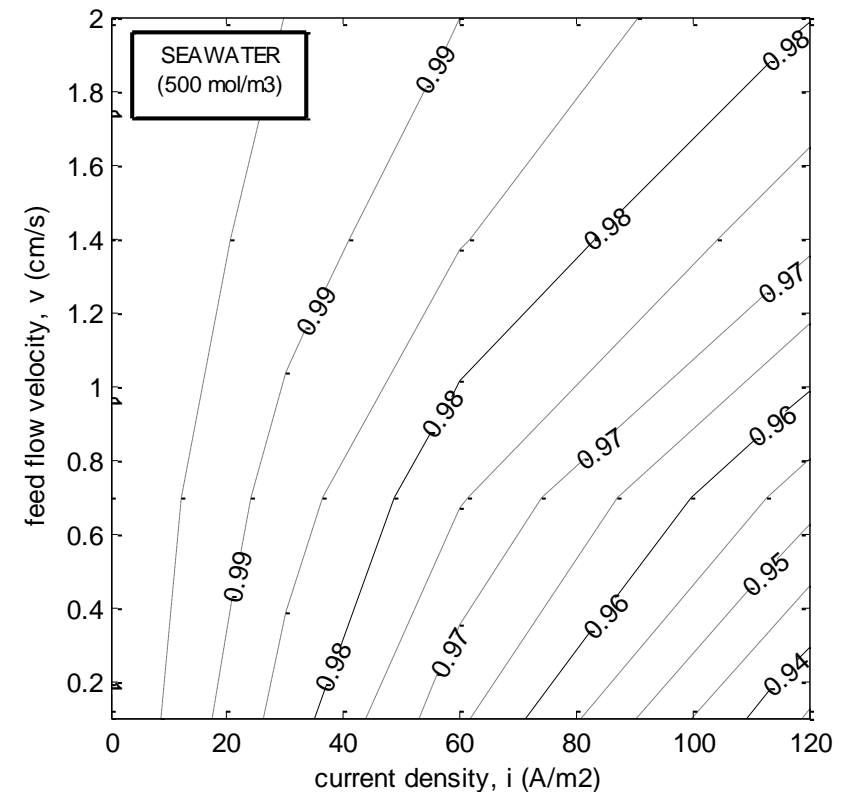
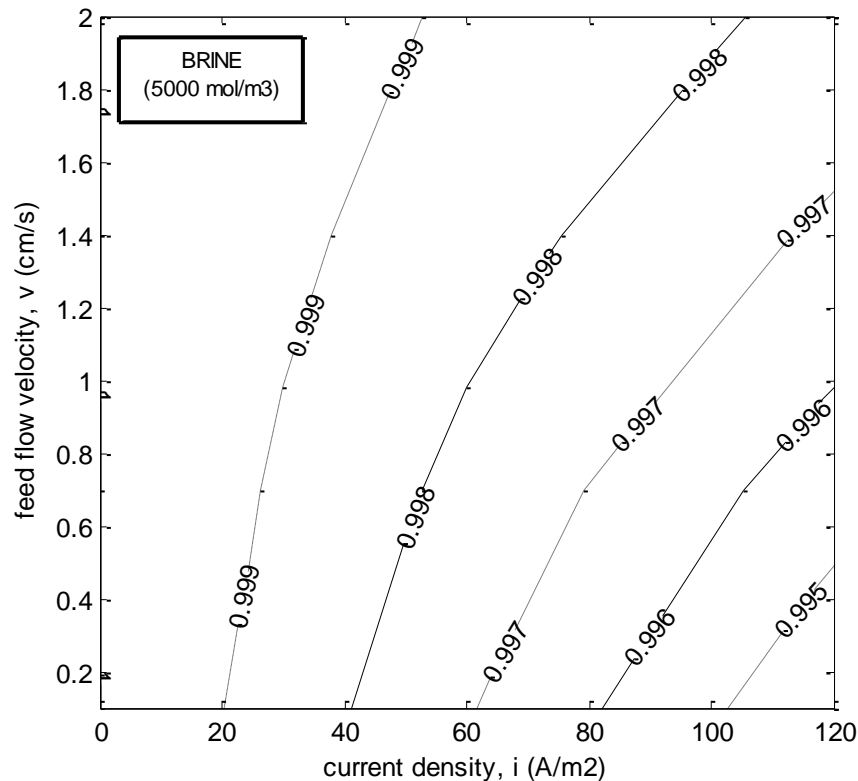
River water 0.017M



- Very high θ values predicted for brine and seawater, lower for river water. If $C \uparrow$, $\theta \uparrow$
- The higher i , the lower the θ value, but this dependence is crucial only for river water
- Higher w corresponds to an enhanced mixing. If $w \uparrow$, $\theta \uparrow$

CFD Modelling: prediction of polarisation phenomena

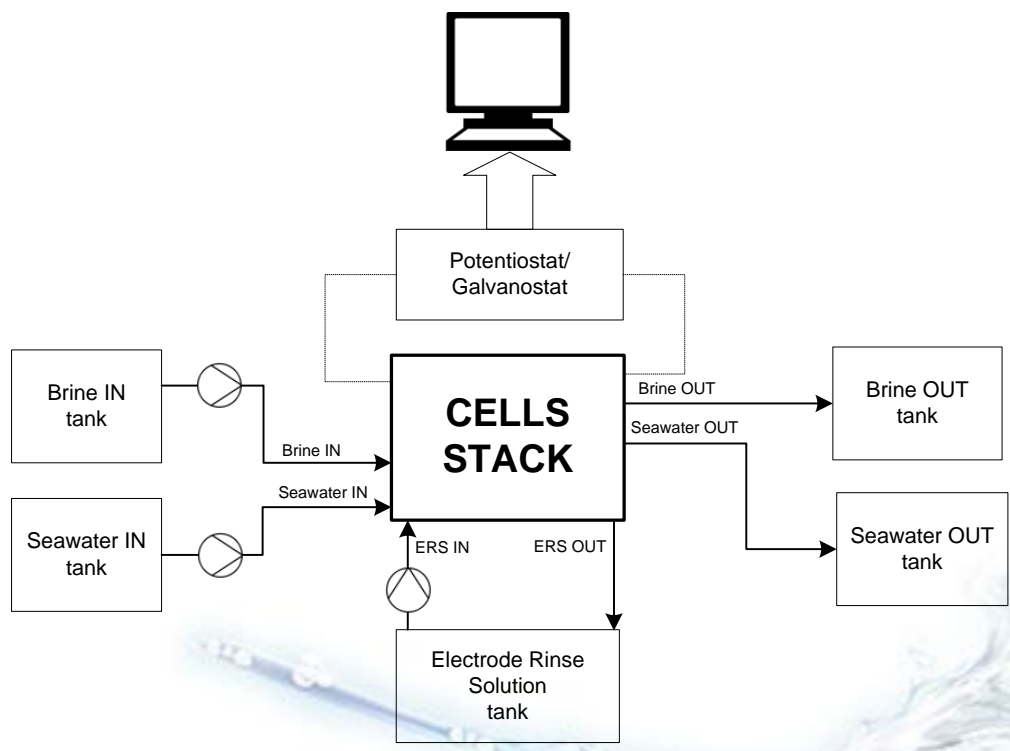
Polarization factor for Deukum spacer-filled channels



Example: Effect of current density and fluid velocity on polarization coefficients.
Model predictions from CFD simulations with 280 μm polyamide woven spacer (Deukum GmbH, Germany).

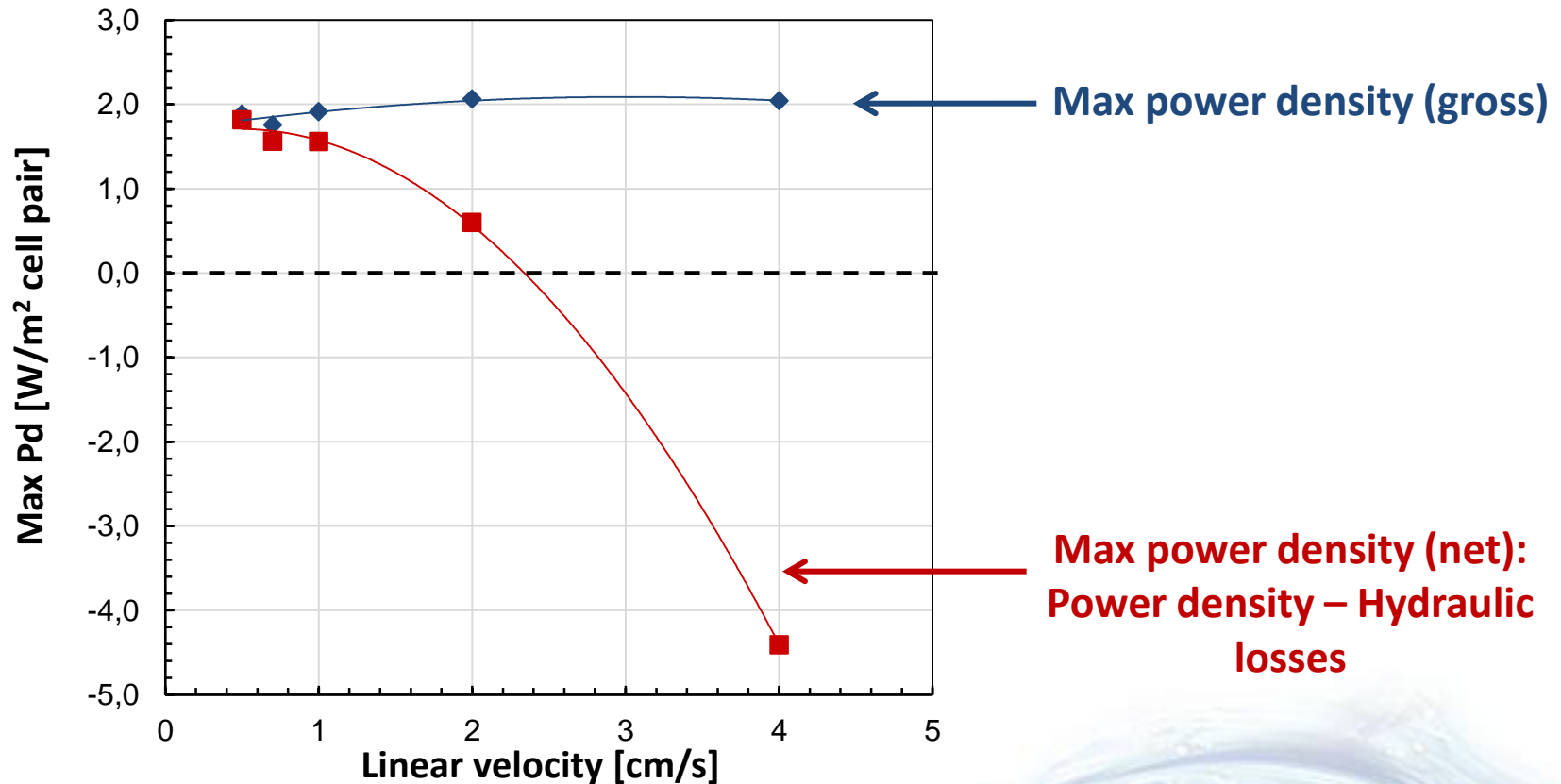
Experiments on the "second generation" stack

An extended experimental campaign has been (and is currently being) carried out at VITO laboratories to investigate the performance of a novel design SGP-RE stack under REAPower conditions



Experiments on the “second generation” stack

Effect of feed flow linear velocity

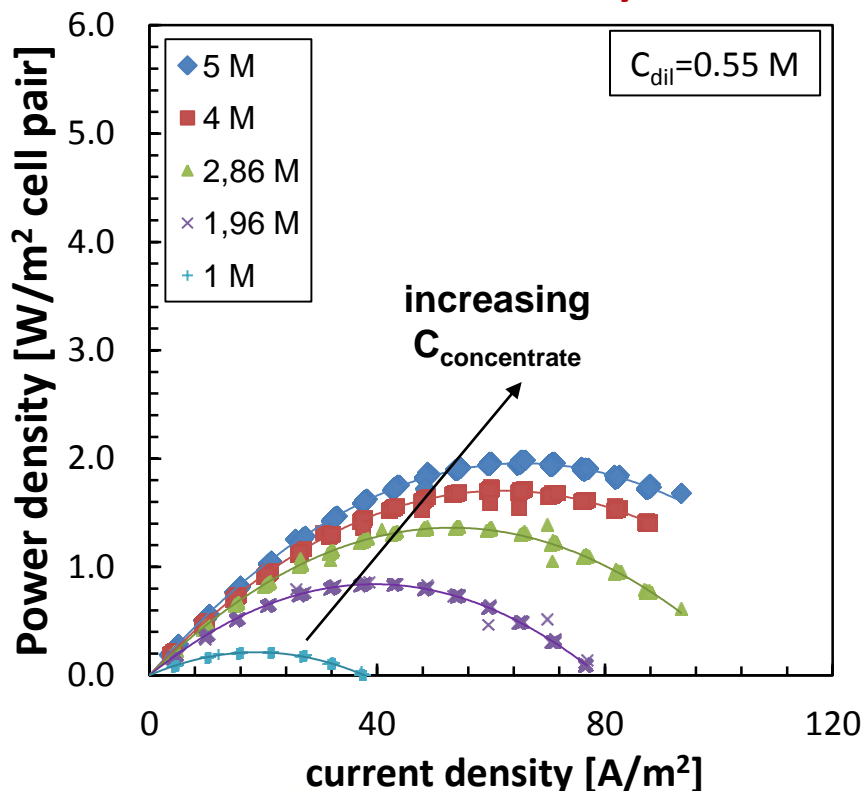


50 cell pairs - 80050 (CEM) and 80045 (AEM) membranes [thickness 120 μ m] - Deukum spacers [thickness 270 μ m] - Brine 5 M, seawater 0,5 M - Electrode rinse solution [(K₃Fe(CN)₆ 0,1 M, K₄Fe(CN)₆ · 3H₂O 0,1M; NaCl 2,5M) –conductivity 204 mS/cm – flow rate 30l/h].

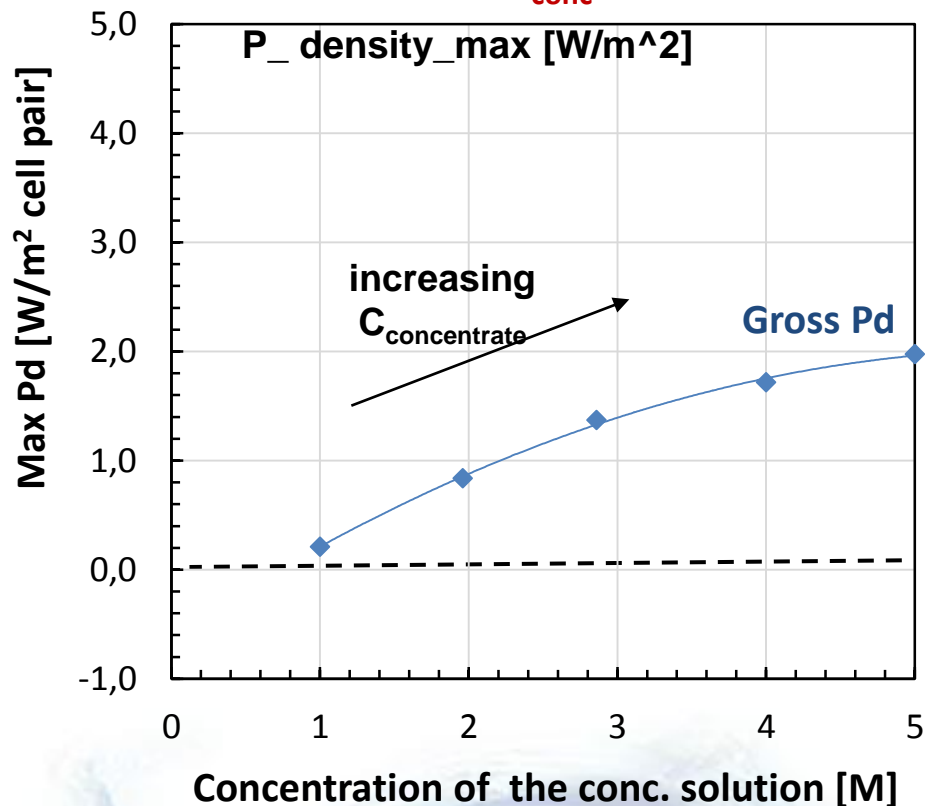
Experiments on the “second generation” stack

Effect of the concentration of the concentrated solution (1 ÷ 5 M)

Power density vs. current density



Maximum power density vs. C_{conc}

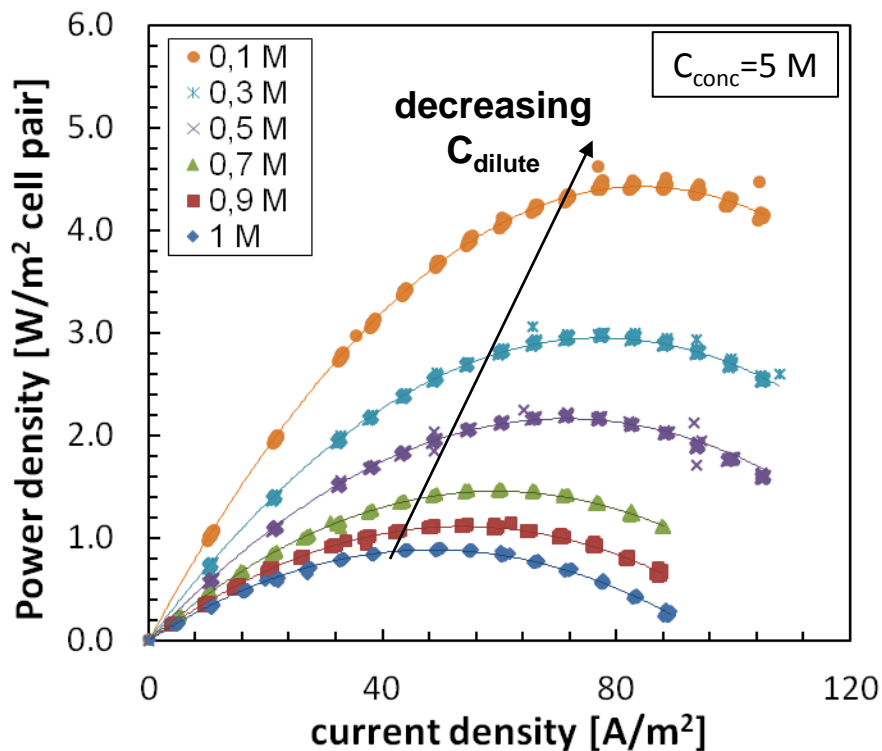


50 cell pairs - 80050 (CEM) and 80045 (AEM) membranes [thickness 120µm] - Deukum spacers [thickness 270 µm] - Brine 5 M [conductivity: 230 mS/cm – linear speed 1cm/s], seawater 0,1 ÷ 0,5 M [conductivity: 10,46 ÷ 84,4 mS/cm – linear speed 1 cm/s] - Electrode rinse solution [($K_3Fe(CN)_6$ 0,1 M, $K_4Fe(CN)_6 \cdot 3H_2O$ 0,1M; NaCl 2,5M) –conductivity 204 mS/cm – flow rate 30l/h].

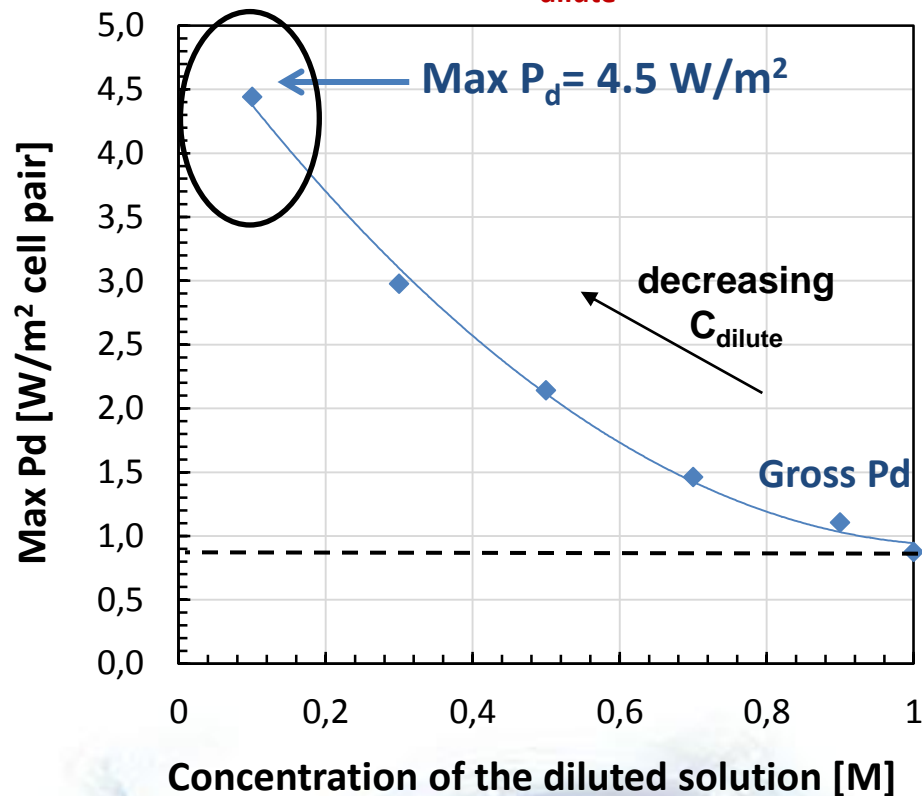
Experiments on the “second generation” stack

Effect of the concentration of the diluted solution (0.1 ÷ 1 M)

Power density vs. current density



Maximum power density vs. C_{dilute}

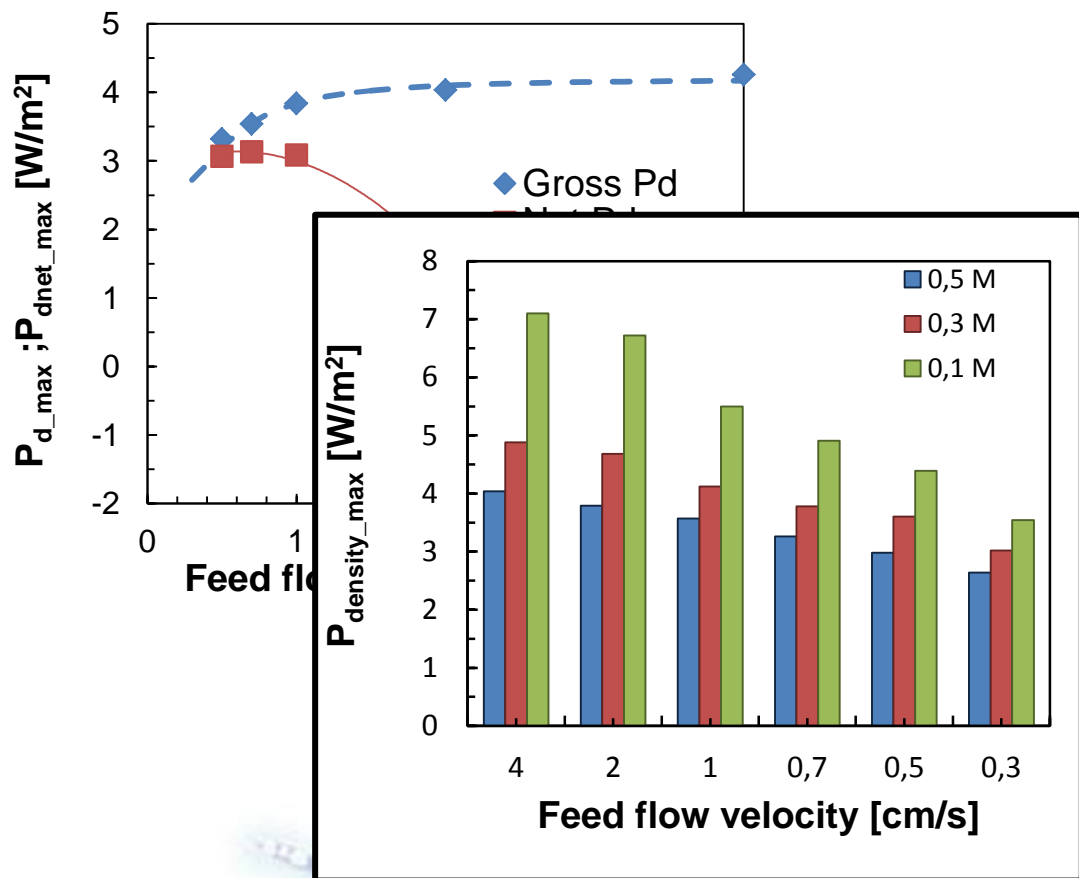


50 cell pairs - 80050 (CEM) and 80045 (AEM) membranes [thickness 120 μ m] - Deukum spacers [thickness 270 μ m] - Brine 5 M [conductivity: 230 mS/cm – linear speed 1cm/s], seawater 0,1 ÷ 0,5 M [conductivity: 10,46 ÷ 84,4 mS/cm – linear speed 1 cm/s] - Electrode rinse solution [($K_3Fe(CN)_6$ 0,1 M, $K_4Fe(CN)_6 \cdot 3H_2O$ 0,1M; NaCl 2,5M) – conductivity 204 mS/cm – flow rate 30l/h].

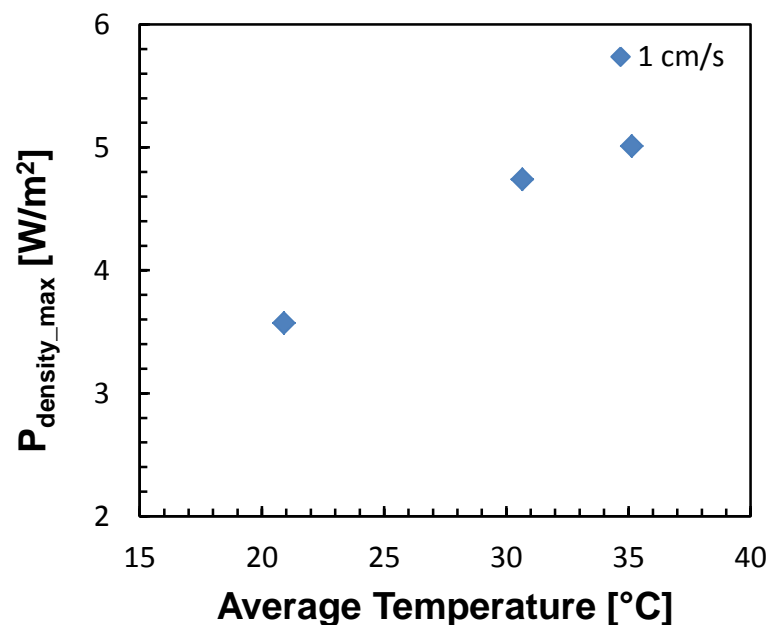
Experiments on the “second generation” stack

Change in membranes: 20-30 μm thin commercial membranes

Influence of flow velocity



Influence of Temperature



Influence of diluate concentration

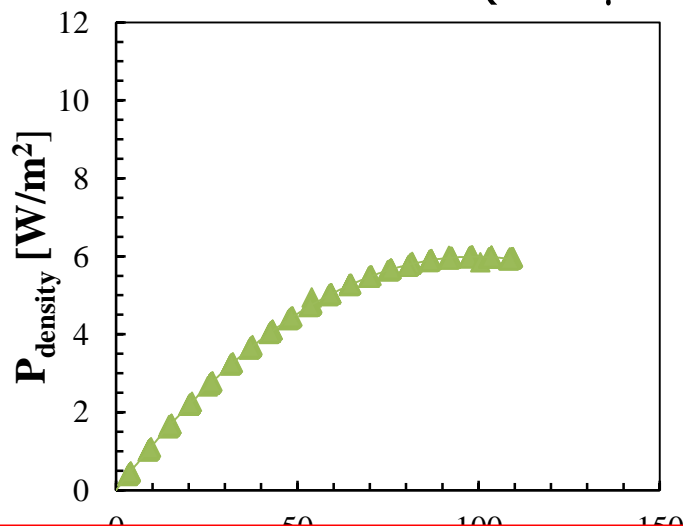
50 cell pairs - FAS – 20/FKS – 20 Fumatech membranes [thickness 20-30 μm] - Deukum spacers [thickness 270 μm] - Brine 5 M, seawater 0,1 ÷ 0,5 M - Electrode rinse solution [(K₃Fe(CN)₆ 0,1 M, K₄Fe(CN)₆ · 3H₂O 0,3M; NaCl 2,5M), flow rate 30l/h].

Experiments on the “second generation” stack

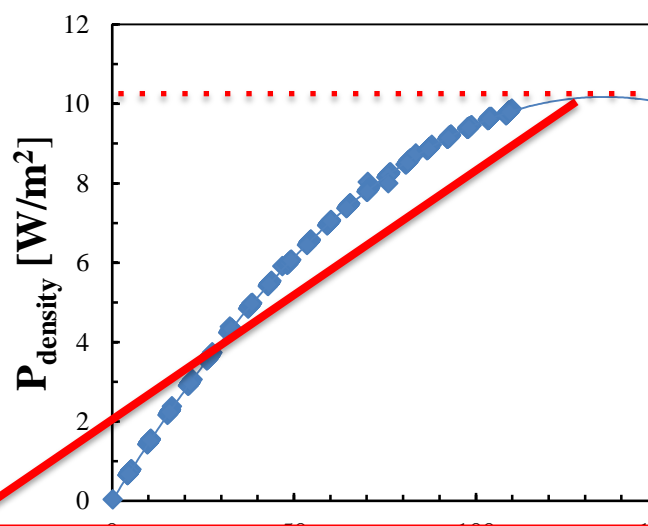
MAX power output conditions:

4cm/s, $T = 40^{\circ}\text{C}$ & brackish water diluate (0.1M)

Thick membranes ($120\mu\text{m}$)

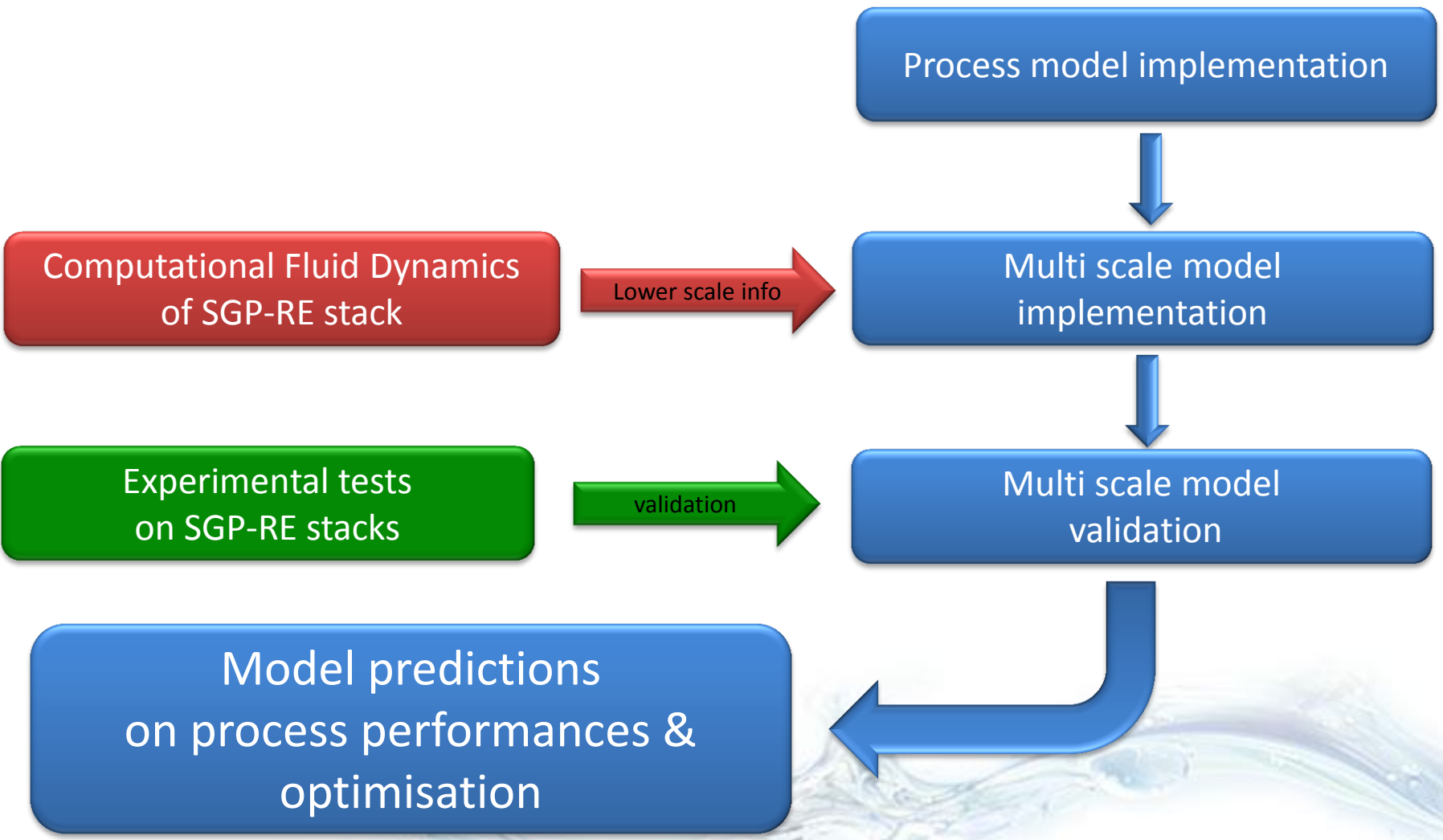


Thin membranes ($20\text{-}30\mu\text{m}$)



A power density between **15 and 20 W/m^2** can be expected with larger number of cell pairs, which would reduce the effect of **blank resistance**

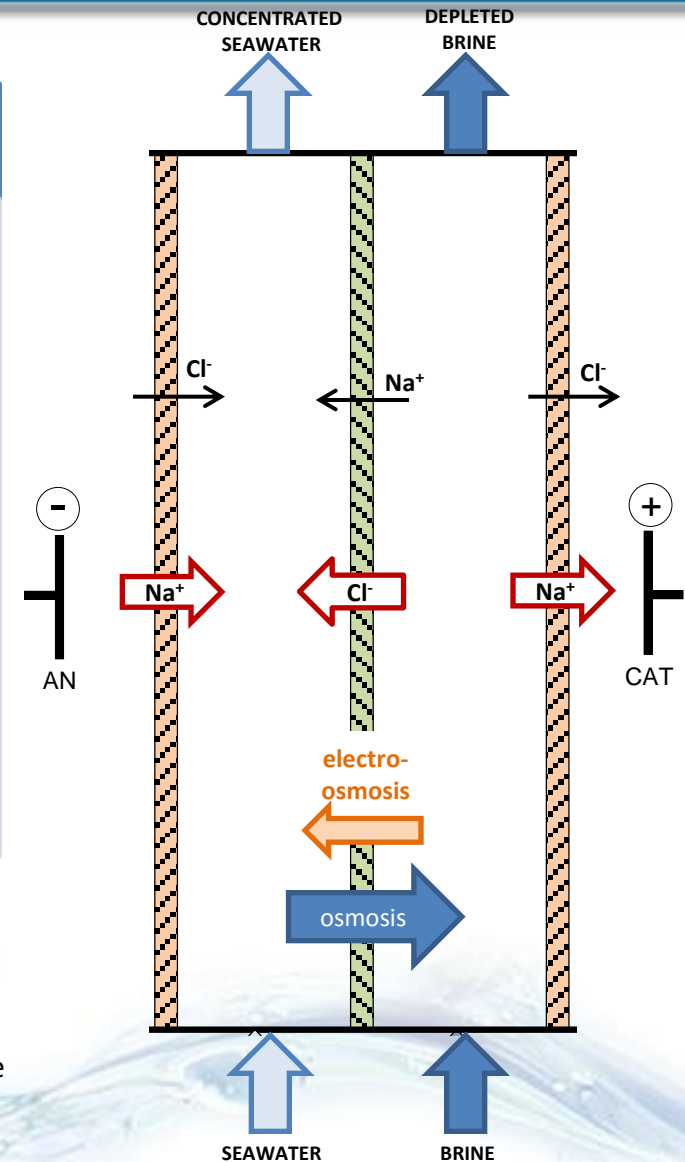
Multi-scale model implementation



Process Modelling Approach

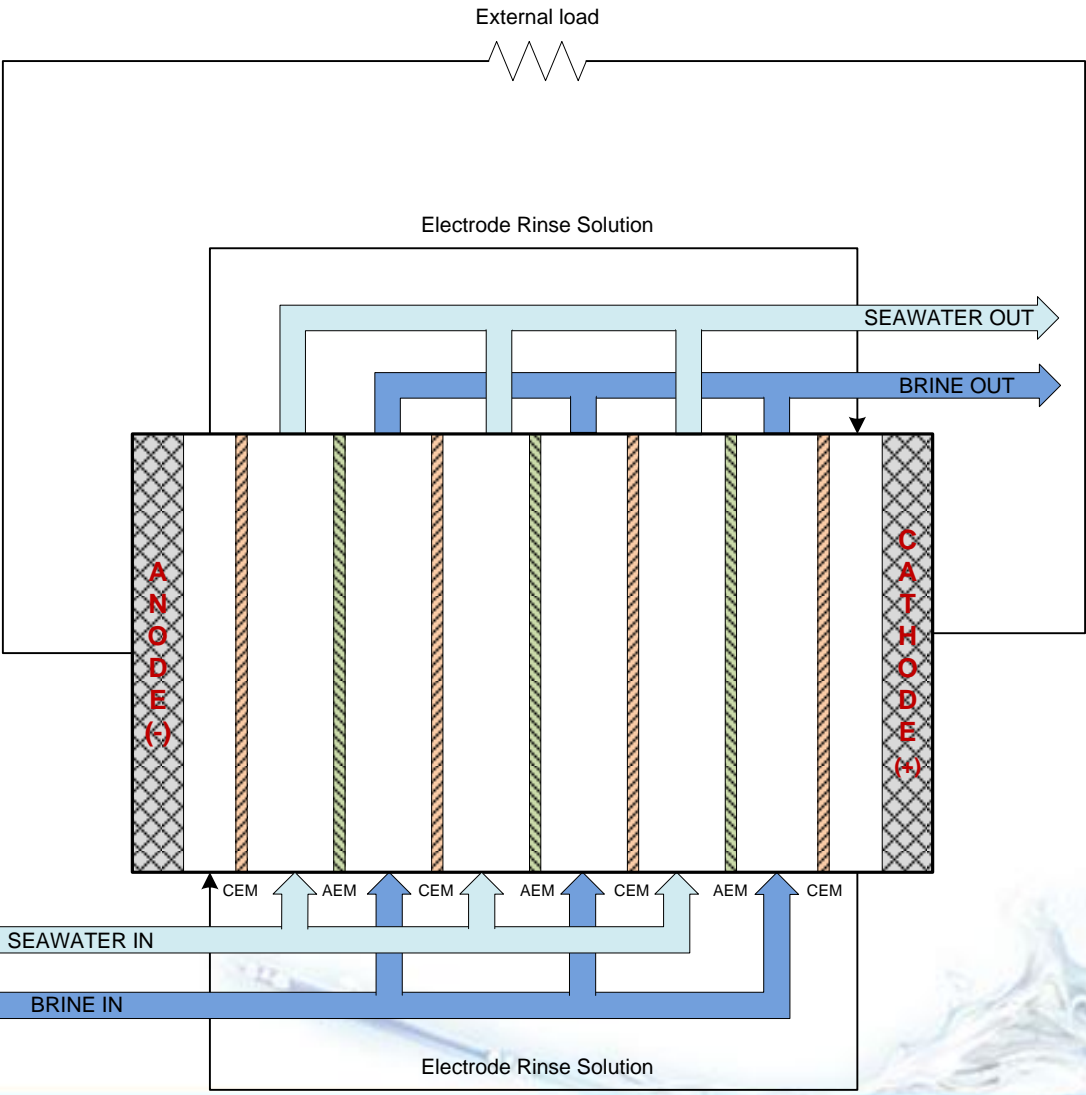
Low-hierarchy model (*cell pair*):

- thermodynamic properties of solutions
- electric variables
- salt transport (counter/co-ions)
- solvent transport (osmosis/electro-osmosis)
- polarization phenomena
- mass balance



Tedesco, M.; Cipollina, A.; Tamburini, A.; van Baak, W.; Micale, G.; "Modelling the Reverse ElectroDialysis process with seawater and concentrated brines", *Desalination and Water Treatment*, vol. 49, pp. 404-424, 2012.

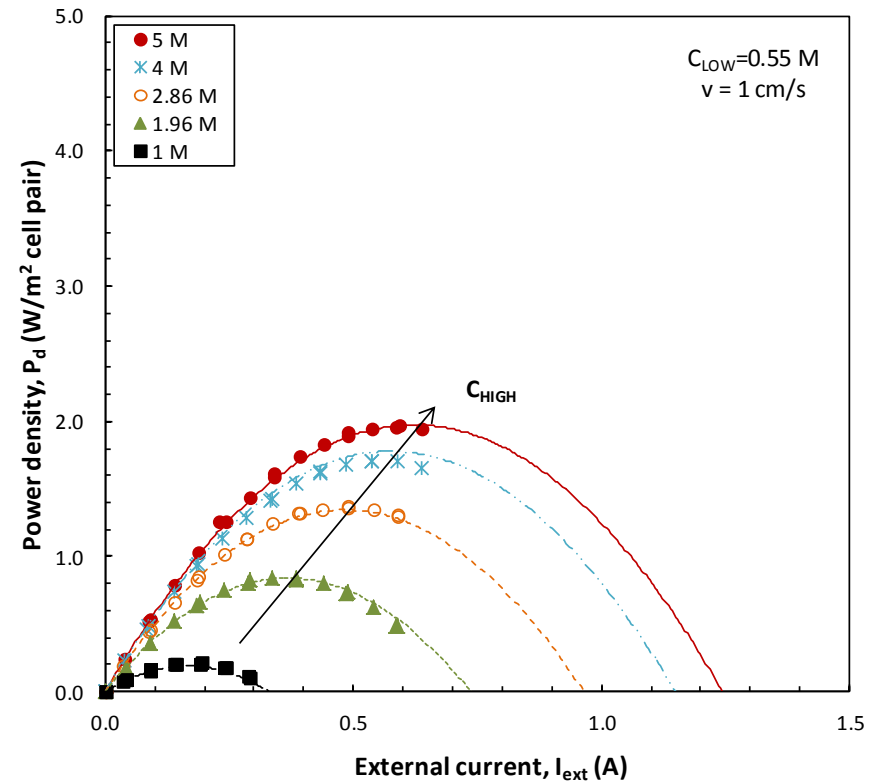
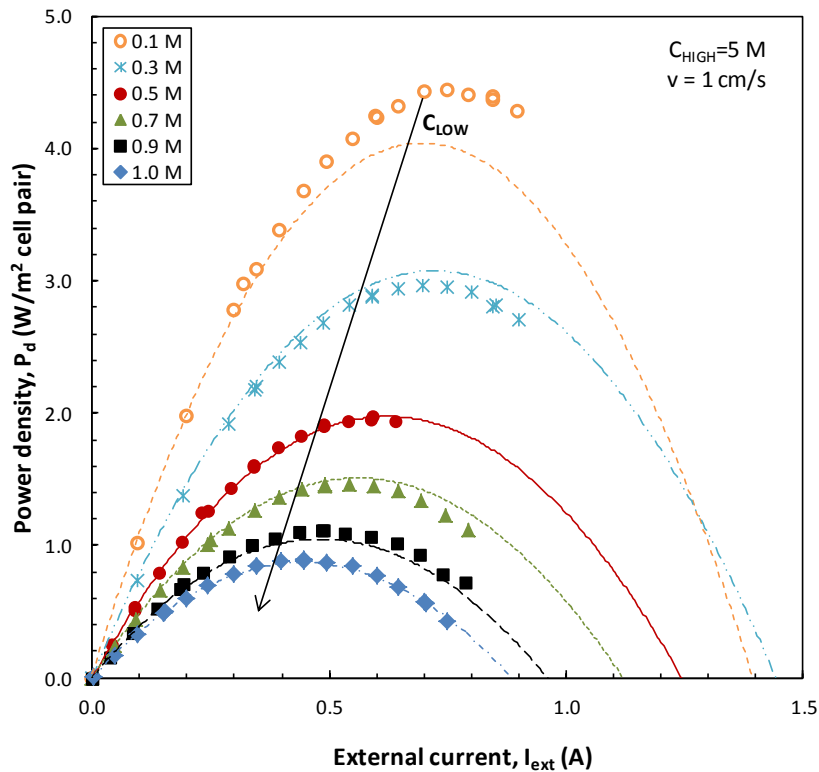
Process Modelling Approach



- High-hierarchy model (*stack*):**
- parasitic currents through manifolds
 - stack resistance
 - stack voltage
 - Pressure drops
 - power density (gross/net)

Process Modelling validation

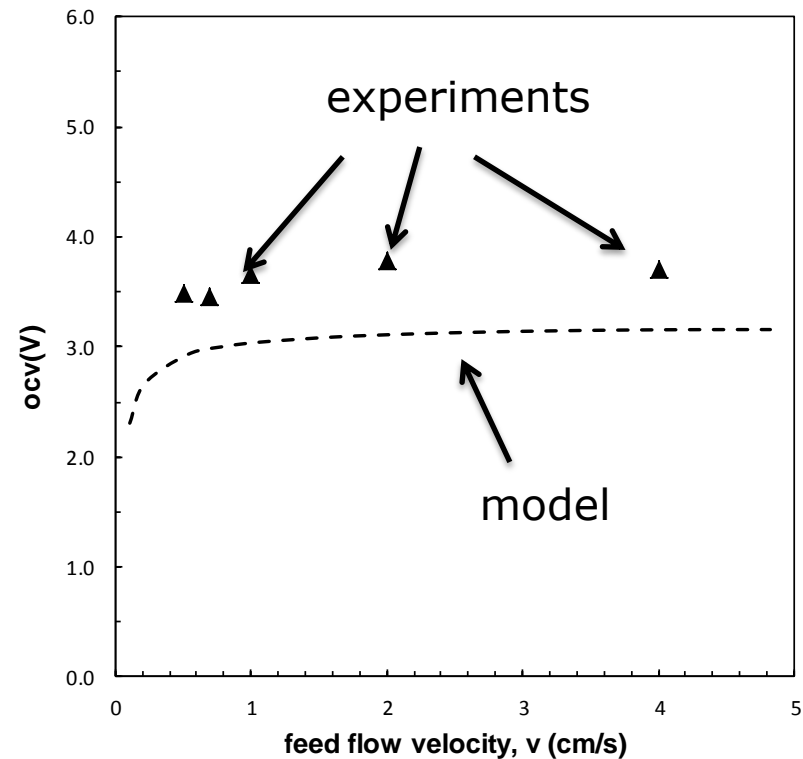
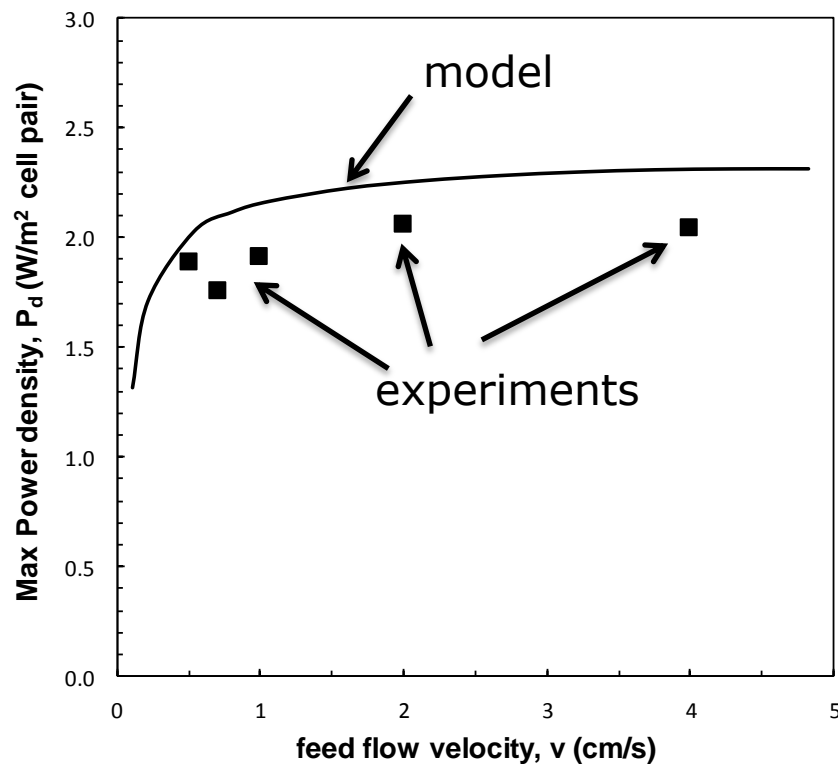
Model calibration with variable feed concentration



Experimental (points) and simulated (lines) data for a 50-cells stack equipped with Fujifilm membranes, Deukum 270 μ m spacers; feed flow velocity: 1 cm/s; $T=20^\circ$ C. Blank resistance: 0.4 Ω . Experimental data collected at VITO (Oct 2012).

Prediction of dependences

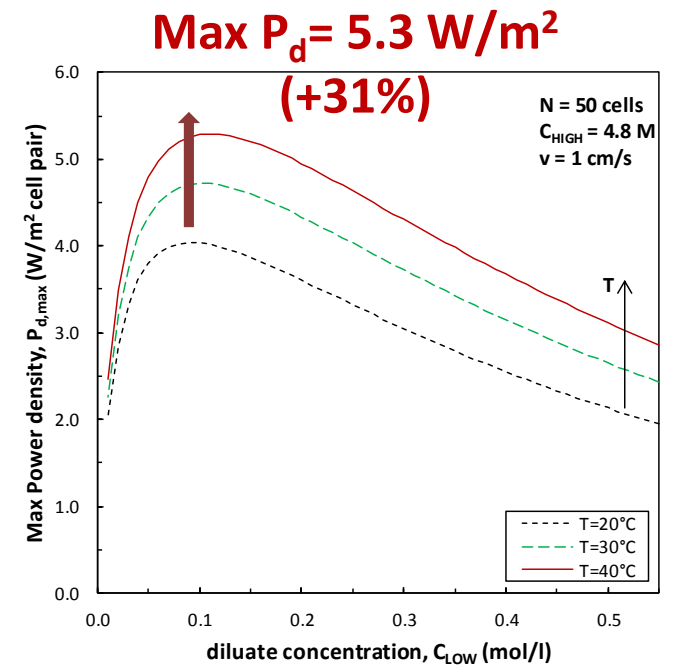
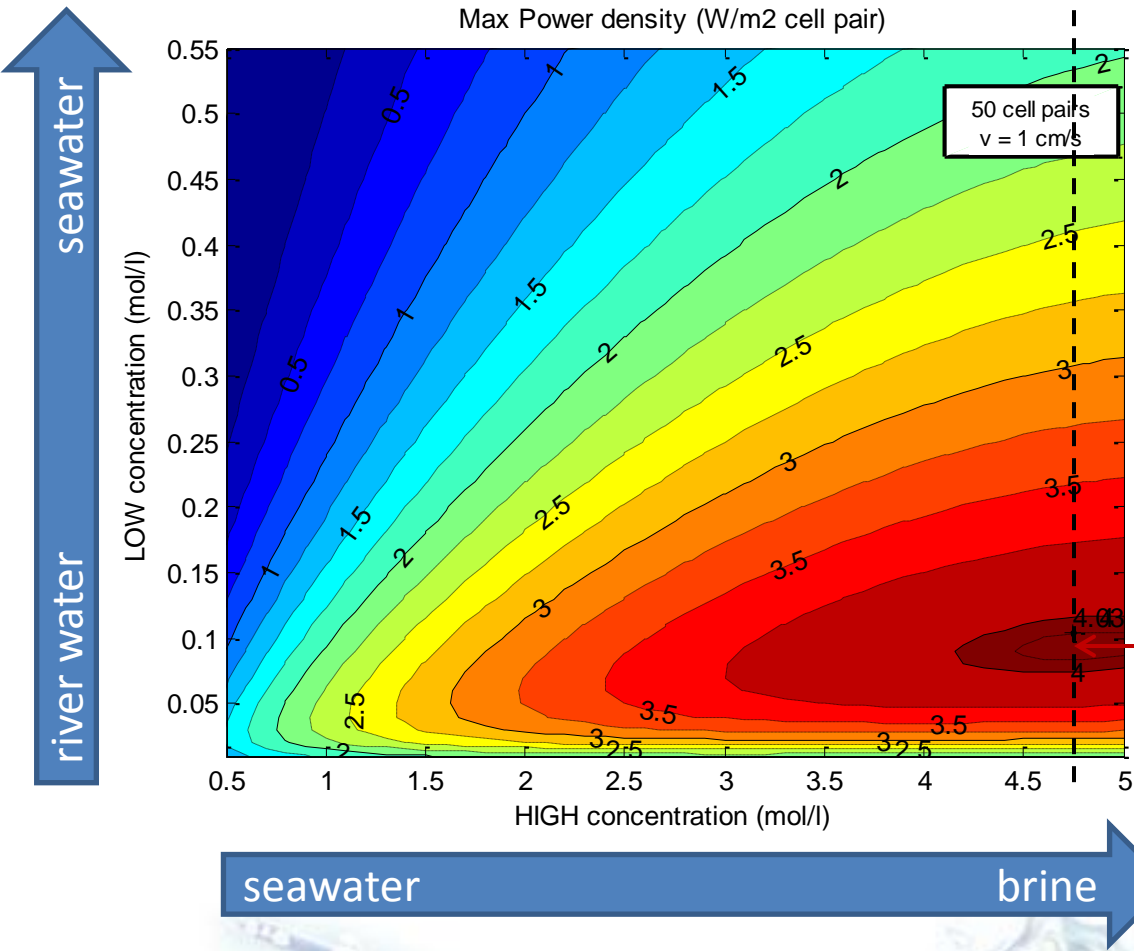
Influence of feed flow rate



Experimental (points) and simulated (lines) data for a 50-cells stack equipped with Fujifilm membranes, Deukum 270 μm spacers. $C_{\text{HIGH}}=5\text{ M}$; $C_{\text{LOW}}=0.5\text{ M}$; $T=20^\circ\text{ C}$. Blank resistance: $0.4\ \Omega$. Experimental measurements collected at VITO (Mar-Apr 2013).

Prediction of dependences

Influence of feed T & conc.

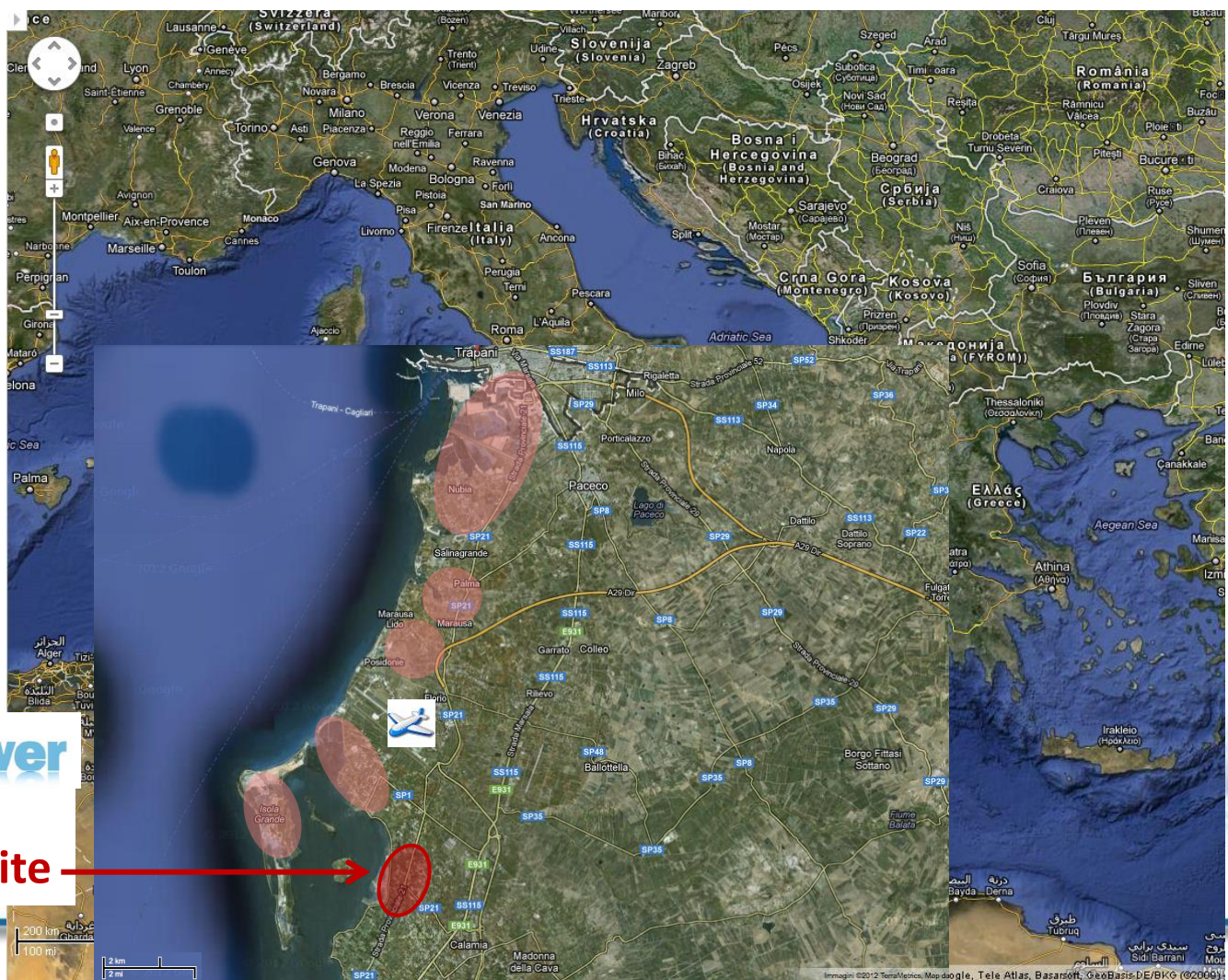


BEST conditions:
brackish water (0.05 – 0.1 M)
+ brine (4.5 – 5 M)

Simulations of a 50-cells stack equipped with Fujifilm membranes, Deukum spacers; feed flow velocity inside channels: 1 cm/s; $T=20^{\circ}C$. Blank resistance: 0.4 Ω .

Which brines for the SGP-RE process?

Prototype installation site: the singular framework of Trapani saltworks



 **REAPower**
Prototype
installation site →

Which brines for the SGP-RE process?

Prototype installation site: Ettore-Infersa saltworks



Direct access to both saturated brine and seawater from open channels

Installation place within an old, restructured WINDMILL



Prototype installation: plant specifications

Site features

- Seawater availability: unlimited;
- Brine availability: 10-15 m³/h (much larger with feed-recycle);
- Brine concentration: variable between 250 and 320 gr/lit.

Provisional Prototype features

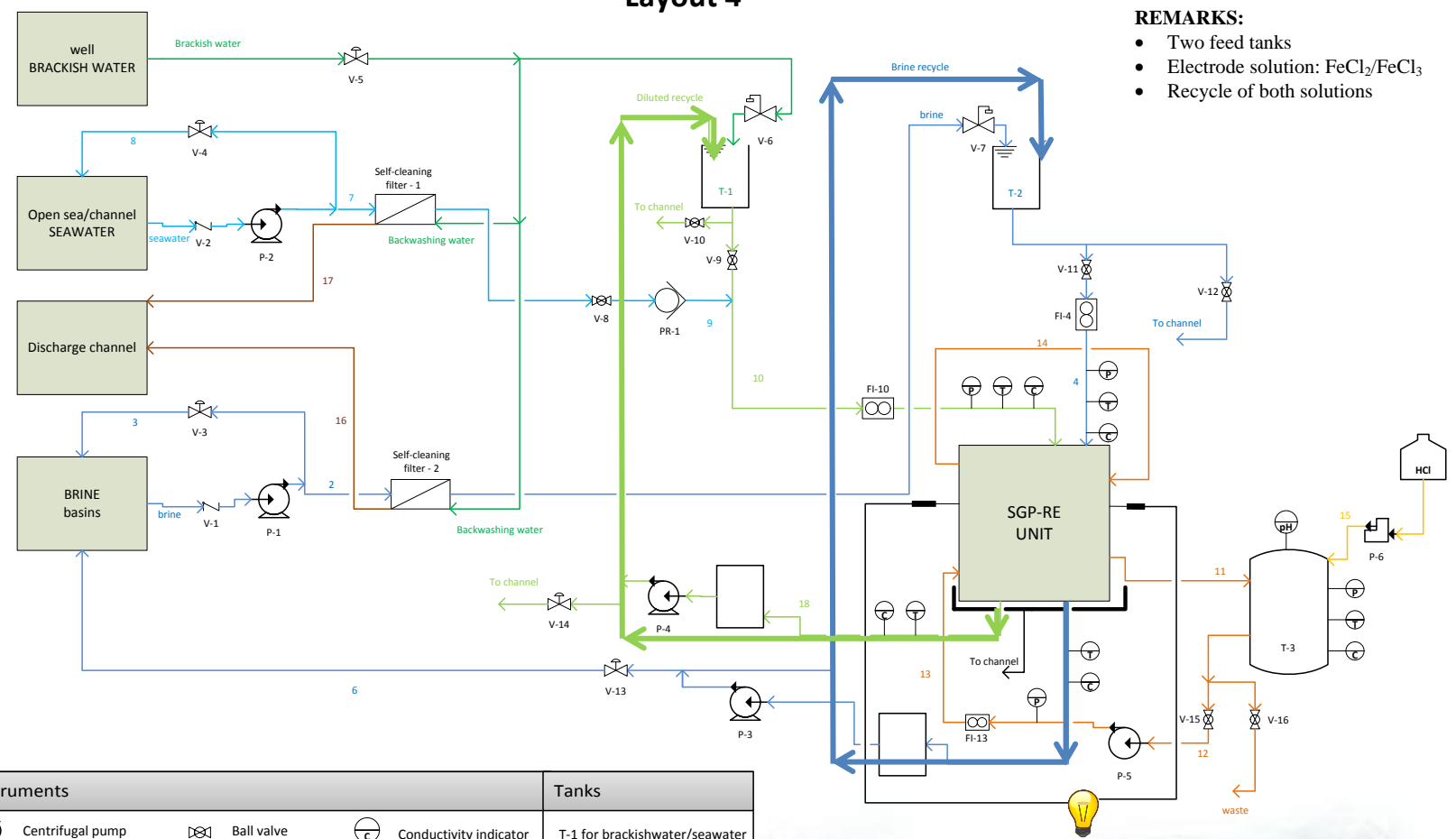
- Total cell pair surface: from 4 to 125m² (2 stacks will be tested);
- Expected power density: > 5 W/m²;
- Expected power output: from 20 to 600W

Process Flow Diagram & recycle option

Layout 4

REMARKS:

- Two feed tanks
- Electrode solution: $FeCl_2/FeCl_3$
- Recycle of both solutions

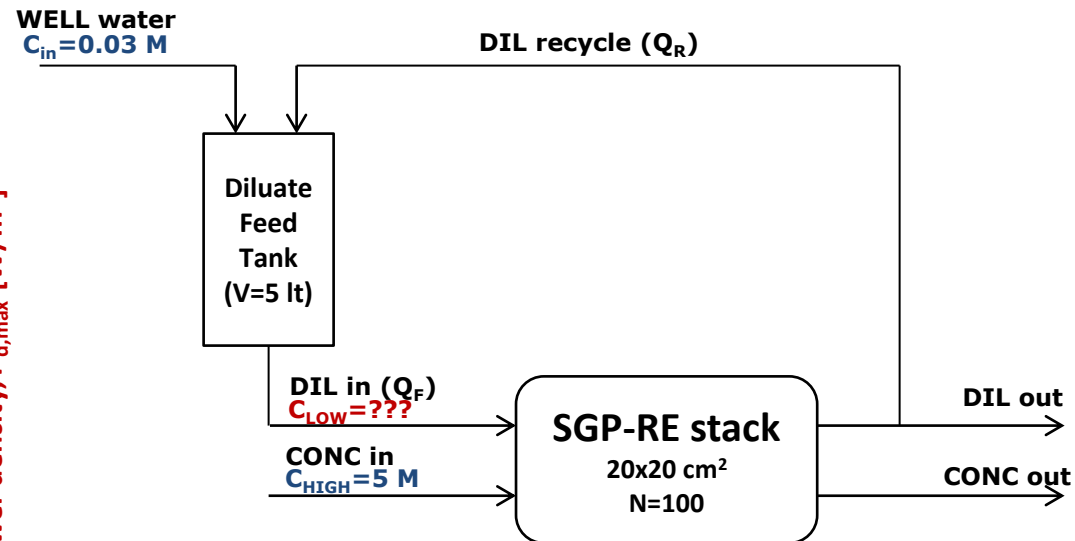
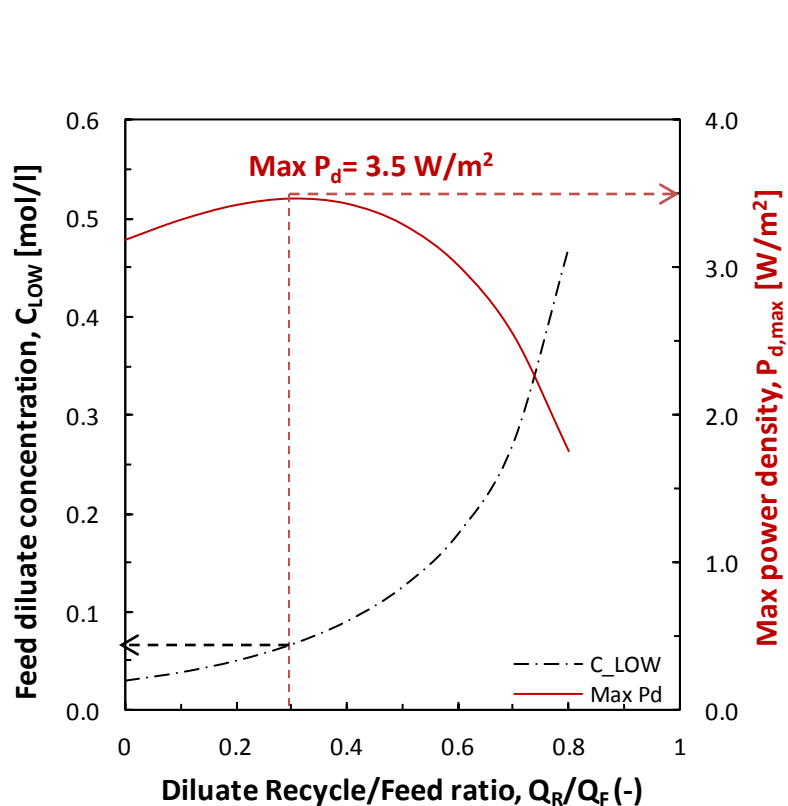


Instruments			Tanks
	Centrifugal pump		T-1 for brackishwater/seawater
	Rotary pump		
	Proportioning pump		
	Check valve		T-2 for brine
	Membrane valve		
	Conductivity indicator		T-3 for electrode solution
	Temperature indicator		
	Pressure indicator		

Scalici Claudio	WP7 Pilot Prototype
Installation site: Ettore-Inferna saltworks	24/05/2013

Simulation of Trapani prototype (2/3)

Investigate the optimal Recycle/Feed ratio for diluate



Simulations of a $20 \times 20 \text{ cm}^2$ stack equipped **100 cells**, Fujifilm membranes, Deukum spacers; feed flow velocity inside channels: 1 cm/s ; $T = 20^\circ \text{ C}$. $C_{HIGH} = 5 \text{ M}$. Blank resistance: 0.4Ω .

REAPower website

<http://www.reapower.eu/>



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The Future

of sustainable energy production



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*Thank you
for your attention*

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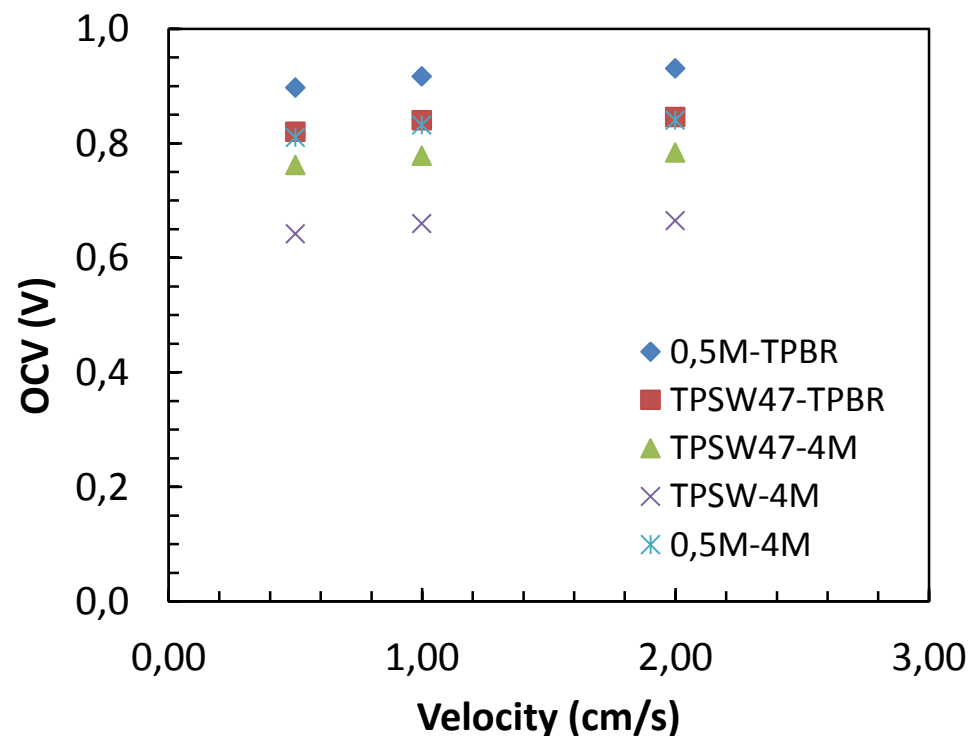
REAPower project is funded by the European Union Seventh Framework Programme (FP7/2007-2013), Future Emerging Technologies for Energy Applications (FET) (Project No FP7-256736). The sole responsibility for the content of this presentation lies with the authors. It does not necessarily reflect the opinion of the European Union. The European Commission cannot be held responsible for any use that may be made of the information contained therein.

ICMAT 2013 - 30 June to 6 July 2013, Suntec Singapore

Back-up slides

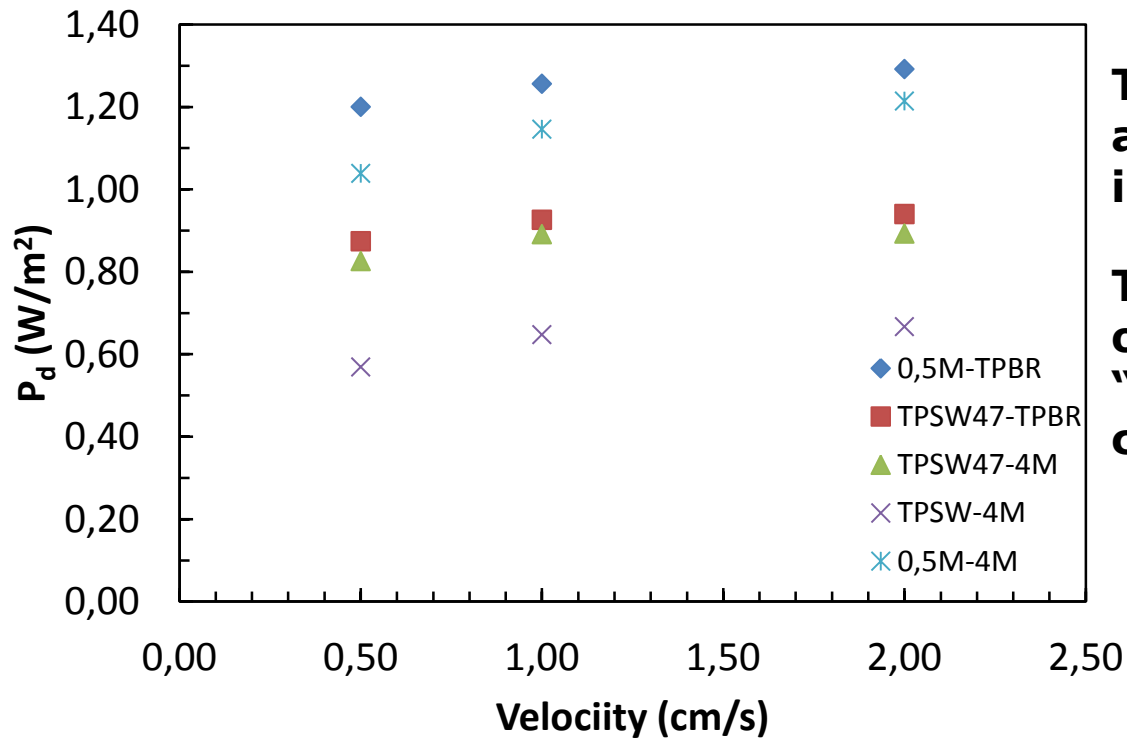
Influence of the use of real solutions on the power density

Name	Description	Conductivity [mS/cm]
0,5M	NaCl solution, 0.5M	47
4M	NaCl solution, 4M	228
TPSW	Seawater from Trapani	
TPBR	Brine from Trapani	
TPSW47	Seawater from Trapani diluted 0,5M solution conductivity	



Back-up slides

Influence of the use of real solutions on the power density

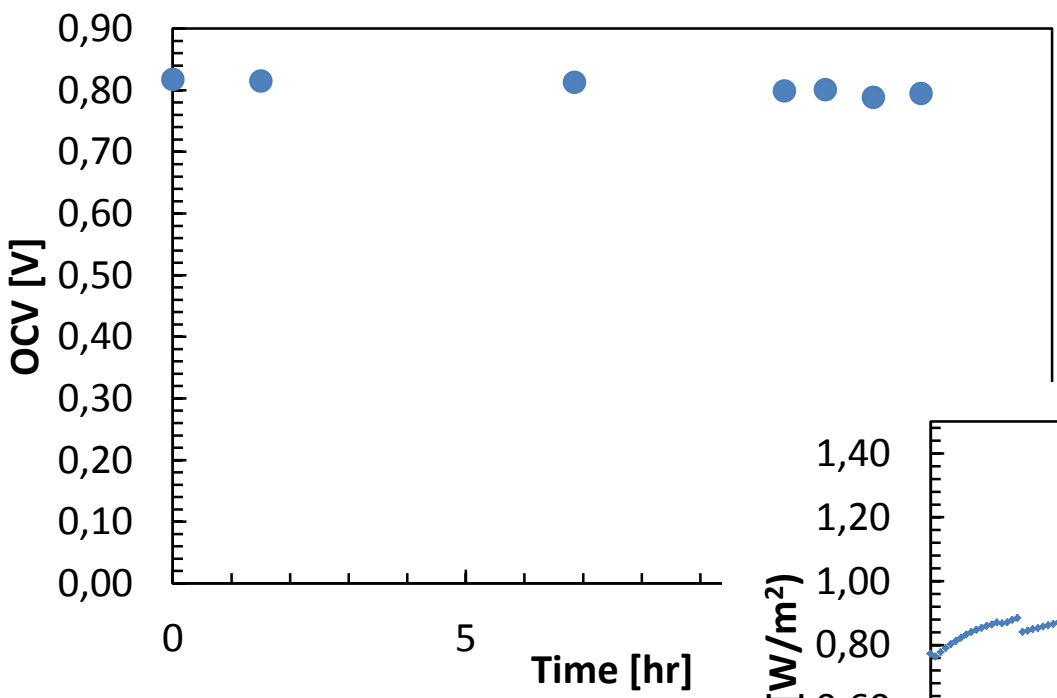


TP brine does not negatively affect the P_d , but a slight increase is observed;

TP SW significantly reduces the obtained P_d , even if "corrected" to the same conductivity as 0,5M solution;

Back-up slides

Long-run test with real solutions (13 hrs test)



No significant variations in the 13 hrs were observed...

